
A Helmholtz energy equation of state for calculating the thermodynamic properties of fluid mixtures

Eric W. Lemmon, Reiner Tillner-Roth

Abstract

- New Approach
 - ▶ based on highly accurate EOS for the pure components combined at the reduced T , ρ of the mixture
 - ▶ reducing parameters for the T, ρ : composition
- For simple mixtures
 - ▶ with relatively simple functions
 - very accurate representation
- For nonideal mixtures
 - ▶ modified reducing func. (T, ρ) + departure func.
 - 0.1% in density, 1% in C_v , 1% in bubble point pressure

Abstract

- Two applications of mixture model concepts
 - ▶ developed independently in USA and Germany over the same time period
 - ▶ including the development of individual equation for each binary system
 - generalization of the model for a wide variety of mixtures
 - ▶ Similarities and differences

Introduction

- Dimensionless Helmholtz energy, $\alpha = A/RT$
 - ▶ Thermodynamic properties of pure fluids with high accuracy over a wide range of T, P
 - ▶ All thermodynamic properties from a single mathematical relation
 - ▶ A large number of adjustable coeff. (up to 58 terms reported)
 - ▶ Reference equation for the calculation of property tables and chart
 - accuracy : restricted only by the accuracy of available measurements

Introduction

- Due to the complexity
 - ▶ Equation with many coefficients
 - applied only to pure fluids
 - ▶ High-accuracy EOS
 - developed for only about 30 pure substances

- Only a few attempts to describe mixture properties using multiparameter EOS

Introduction

- Plocker et al. (1978)
 - ▶ one-fluid theory applied to modified Benedict-Webb-Rubin(mBWR) EOS
 - ▶ with a mixing rule for the pseudo-critical temperature
 - ▶ VLE and Enthalpies at high pressures
- Platzer and Maurer (1993)
 - ▶ generalized the 20-term Bender equation
 - ▶ prediction for multicomponents mixture properties
- Huber and Ely (1994)
 - ▶ extended corresponding states model based on mBWR EOS

Introduction

- Mixture model (pure \rightarrow mixture)
 - ▶ based on high-accuracy pure fluid EOS for the pure components
 - ▶ pressure-explicit EOS
 - simple integration of pressure
 - * generally explicit in Helmholtz energy
 - ▶▶ adopted for the mixture
 - ▶ combination rules for the Helmholtz energy function of mixture components (not mixing rules)
 - not required a fixed structure of the pure fluid equation
 - ▶ single mathematical expression

Introduction

- General form of Helmholtz energy model
 - ▶ independently developed by both authors during overlapping periods of time
- Tillner-Roth (1993)
 - ▶ focused on developing an accurate formulation for individual binary mixtures for a large amount of accurate experimental data
- Lemmon (1996)
 - ▶ focused on developing a generalized model capable of accurate property calculation for a large number of fluid mixtures

Introduction

- Purpose

- ▶ additional detail and background for the models
 - especially ideal mixture
- ▶ difference between the models

Helmholtz energy

- EOS for the pure fluids

- ▶ ideal part + residual part

$$\frac{A}{RT} = \alpha(\tau, \delta) = \alpha^0(\tau, \delta) + \alpha^r(\tau, \delta)$$

$$\alpha^0(\tau, \delta) = \ln \delta + c_1 \ln \tau + \sum_{k=2}^{k1} c_k \tau^{m_k} + \sum_{k=k1+1}^{k2} c_k \ln[1 - \exp(-a_k \tau)]$$

$$\alpha^r(\tau, \delta) = \sum_{k=k2+1}^{k3} c_k \delta^{n_k} \tau^{m_k} + \sum_{k=k3+1}^{k4} c_k \delta^{n_k} \tau^{m_k} \exp(-\delta^{e_k})$$

$$\tau = \frac{T_n}{T}, \delta = \frac{\rho}{\rho_n} = \frac{V_n}{V}$$

- ▶ reducing parameter T_n , V_n : critical properties

Helmholtz energy

- Transforming into the Helmholtz energy form by integrating the relation

$$p = \rho RT \left[1 + \delta \left(\frac{\partial \alpha^r}{\partial \delta} \right)_\tau \right]$$

Mixture Model

- α of mixture : composition dependence

$$\alpha = \alpha^0 + \alpha^r$$

- Ideal gas mixture : analytically from functions for the ideal gas properties of the pure fluids

$$\alpha^0 = \alpha^0(T, V, \mathbf{x}) = \sum_{i=1}^l x_i \alpha_i^0(T, V) + \sum_{i=1}^l x_i \ln x_i$$

- ▶ consistent with ideal parts of the pure fluid equation with independent reduced variable τ , δ

Mixture Model

- Residual Helmholtz energy

$$\alpha^r(\tau, \delta, \mathbf{x}) = \sum_{i=1}^l x_i \alpha_i^r(\tau, \delta) + \Delta\alpha^r(\tau, \delta, \mathbf{x})$$

- ▶ linear combination of the pure fluid residual energy
- ▶ departure function, $\Delta\alpha^r$
 - interaction of different species in the mixture
- ▶ Corresponding states principle
 - shape factors : ratios of the critical properties

$$T_r = T \cdot h = T \frac{T_{n,r}}{T_n}, \quad \tau_r = \frac{T_{n,r}}{T_r} = \frac{T_n}{T} = \tau$$

Mixture Model

Table 1

Thermodynamic properties calculated from the Helmholtz energy model [abbreviations: $\alpha_\delta^r = (\partial\alpha^r/\partial\delta)_{\tau,x}$, $\alpha_\tau^r = (\partial\alpha^r/\partial\tau)_{\delta,x}$, $\alpha_{\delta\delta}^r = (\partial^2\alpha^r/\partial\delta^2)_{\tau,x}$, $\alpha_{\tau\tau}^r = (\partial^2\alpha^r/\partial\tau^2)_{\delta,x}$, $\alpha_{\delta\tau}^r = (\partial^2\alpha^r/\partial\delta\partial\tau)_x$, $\delta = \delta(x)$, $\tau = \tau(x)$]

Ideal gas properties

Internal Energy	$U^0/RT = \sum_{i=1}^I x_i \tau_i (\partial\alpha_i^0/\partial\tau_i)$
Enthalpy	$H^0/RT = 1 + \sum_{i=1}^I x_i \tau_i (\partial\alpha_i^0/\partial\tau_i)$
Entropy	$S^0/R = \sum_{i=1}^I x_i \tau_i (\partial\alpha_i^0/\partial\tau_i) - \alpha^0$
Isochoric heat capacity	$C_V^0/R = -\sum_{i=1}^I x_i \tau_i^2 (\partial^2\alpha_i^0/\partial\tau_i^2)$

Real gas properties

Compressibility factor	$Z = pV/RT = 1 + \delta\alpha_\delta^r$
Fugacity of component i	$f_i = x_i \rho RT \exp(\partial(n\alpha^r)/(\partial n_i))_{T,nV,n_j}$
Internal energy	$U/RT = (U^0/RT) + \tau\alpha_\tau^r$
Enthalpy	$H/RT = (H^0/RT) + \tau\alpha_\tau^r + \delta\alpha_\delta^r$
Entropy	$S/R = (S^0/R) + \tau\alpha_\tau^r - \alpha^r$
Isochoric heat capacity	$C_V/R = (C_V^0/R) - \tau^2\alpha_{\tau\tau}^r$
Isobaric heat capacity	$C_p/R = (C_V/R) + ([1 + \delta\alpha_\delta^r - \delta\tau\alpha_{\delta\tau}^r]^2 / [1 + 2\delta\alpha_\delta^r + \delta^2\alpha_{\delta\delta}^r])$
Speed of sound	$w^2 M/RT = (C_p/C_V)[1 + 2\delta\alpha_\delta^r + \delta^2\alpha_{\delta\delta}^r]$

Mixture Model

- Reducing parameter of the pure fluid equation
≠ reducing functions of the mixture
 - ▶ *pseudo-critical* parameter τ , δ
 - composition dependence

$$\tau(\mathbf{x}) = \frac{T_n(\mathbf{x})}{T}, \delta(\mathbf{x}) = \frac{V_n(\mathbf{x})}{V}$$

→ as x_i approaches 1

$$T_n(\mathbf{x}) \rightarrow T_{n,i}, V_n(\mathbf{x}) \rightarrow V_{n,i}$$

or

$$\tau(\mathbf{x}) \rightarrow \tau_i, \delta(\mathbf{x}) \rightarrow \delta_i$$

Linear mixture model

- Linear mixture model

- ▶ linear combinations of the pure fluid parameters

$$T_n(\mathbf{x}) = \sum_{i=1}^l x_i T_{n,i}, \quad V_n(\mathbf{x}) = \sum_{i=1}^l x_i V_{n,i}$$

- ▶ departure function $\Delta\alpha^r$ omitted
 - ➔ no adjustable parameters

Linear mixture model : Application

- 1,1,1,2-tetrafluoroethane(R-134a)
+difluoromethane(R-32)
 - close behavior of an ideal solution
 - ▶ VLE : excellent results (Fig.1a)
 - ▶ Density in subcritical range (Fig.2a)
 - vapor, liquid density : good agreement
 - ▶ Density in supercritical range (Fig.2b)
 - larger deviation
 - ▶ Isochoric heat capacity
 - $\pm 1\%$ (about the experimental uncertainty)

Linear mixture model : Application

- water+ammonia
 - mixture of polar components showing large mixing effects, wide two-phase region
 - ▶ VLE (Fig.1b)
 - dew curve : well
 - *high conc. in the vapor phase → ideal at lower pressures
 - bubble curve : large deviation
 - ▶ Density (Fig.2c)
 - -1% ~ +3% deviation
 - ▶ Excess enthalpy (Fig.3c)
 - poor representation : related to VLE

Linear mixture model : Application

- ethane+carbon dioxide
 - azeotropic behavior
 - ▶ VLE (Fig.1c)
 - incorrect prediction
 - ▶ Isochoric heat capacity (Fig.3b)
 - less accurate
 - >2% deviation outside of the critical region

Linear mixture model : Application

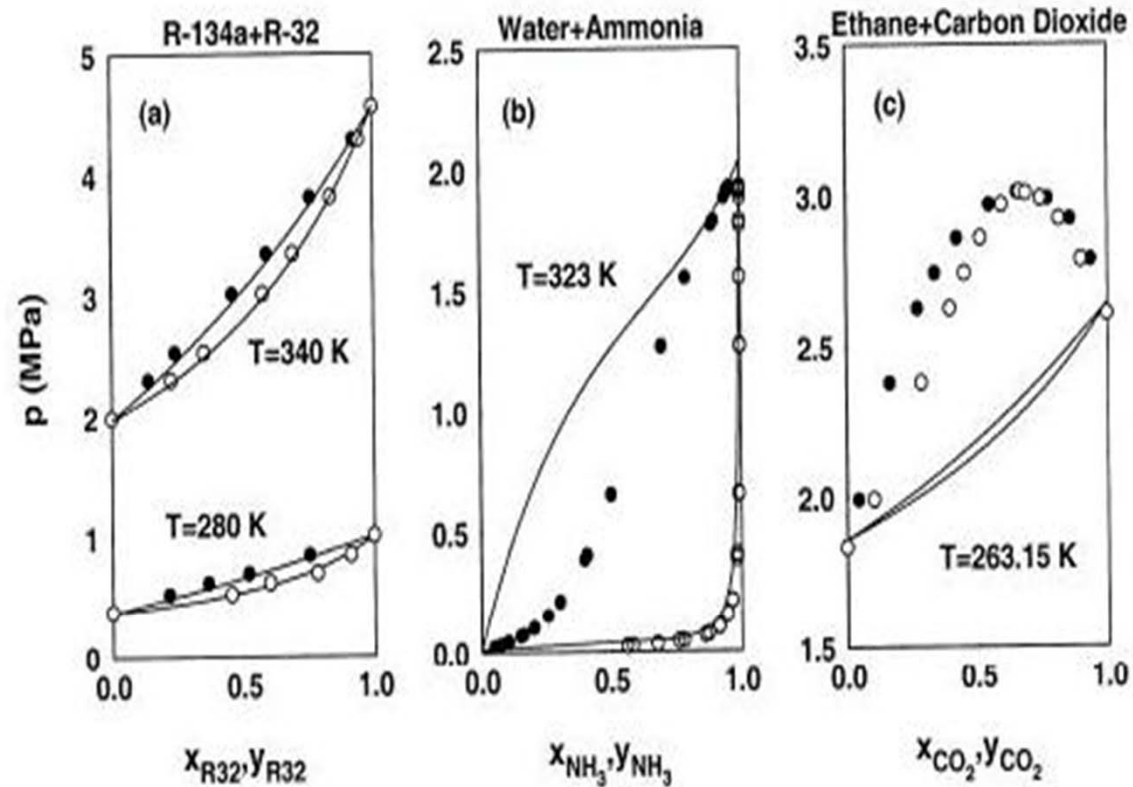


Fig. 1. Experimental and calculated VLE state points from the linear mixture model. (a) R-134a + R-32: \circ , \bullet Holcomb et al. [6]. (b) Water + ammonia: \circ , \bullet Smolen et al. [26]. (c) Ethane + carbon dioxide: \circ , \bullet Fredenslund and Mollerup [3].

Linear mixture model : Application

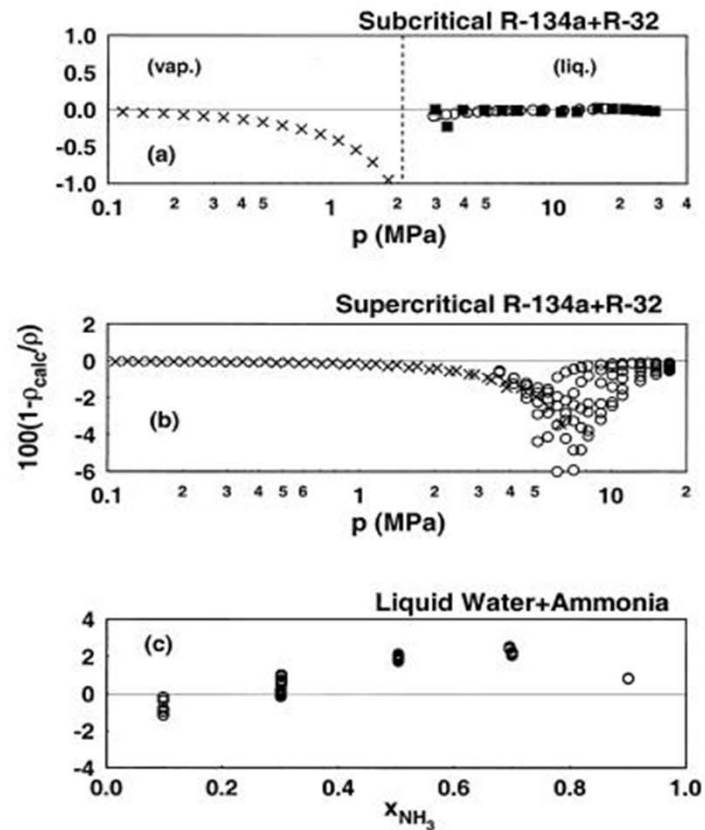


Fig. 2. Density deviations between experimental data and densities calculated from the linear mixture model. (a) Subcritical R-134a+R-32 ($T = 333.15$ K, $x \approx 0.5$): \times , \circ Kleemiss [9]; \blacksquare Magee and Haynes [15]. (b) Supercritical R-134a+R-32 ($363 < T$ (K) < 413 , $x \approx 0.5$): \times , \circ Kleemiss [9]. (c) Liquid water+ammonia ($273 < T$ (K) < 333 , $p < 40$ MPa): \circ Harms-Watzenberg [5].

Linear mixture model : Application

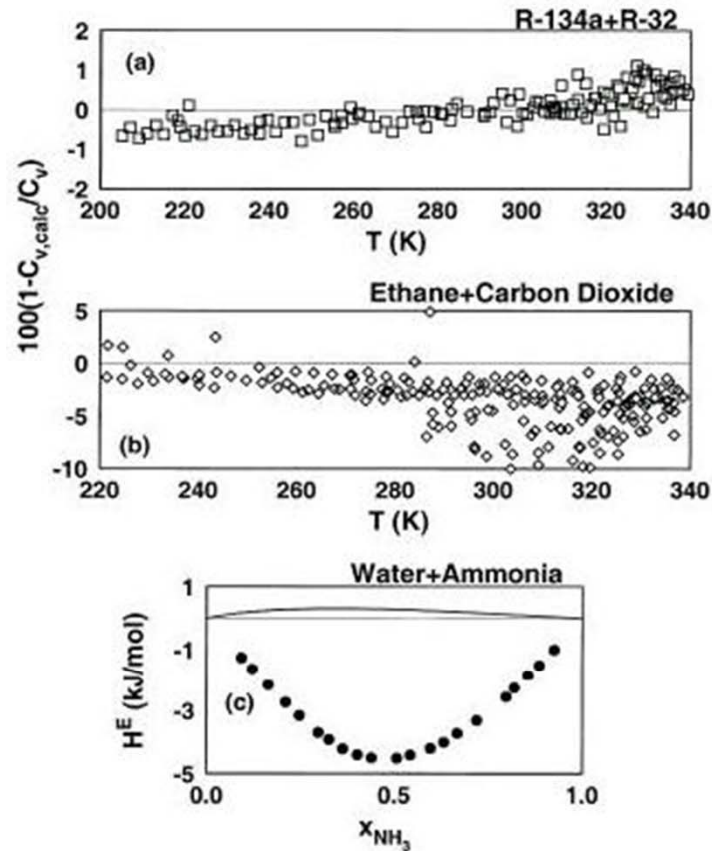


Fig. 3. Deviations between measured caloric properties and values calculated from the linear mixture model. (a) Liquid R-134a + R-32 C_v ($x \approx 0.5$): \square Magee and Haynes [15]. (b) Isochoric heat capacity for ethane + carbon dioxide: \diamond Magee [13]. (c) Excess enthalpy in liquid water + ammonia ($T = 298.15$ K, $p = 5$ MPa): \bullet Staudt [28].

Enhancement to the Mixture Model

- Modification of the reducing functions

$$T_n(\mathbf{x}) = \sum_{i=1}^l \sum_{j=1}^l x_i x_j T_{n,ij}$$

$$T_{n,ij} = k_{T,ij} \frac{1}{2} (T_{n,ii} + T_{n,jj})$$

$$V_n(\mathbf{x}) = \sum_{i=1}^l \sum_{j=1}^l x_i x_j V_{n,ij}$$

$$V_{n,ij} = k_{V,ij} \frac{1}{2} (V_{n,ii} + V_{n,jj})$$

- ▶ $k_{T,ij}$, $k_{V,ij}$: adjustable parameter
- ▶ Effect of varying $k_{T,ij}$, $k_{V,ij}$
 - VLE of ethane+carbon dioxide (Fig.4) ($k_{T,ij} > k_{V,ij}$)
 - C_v : 1.4% deviation (Fig.5)

Enhancement to the Mixture Model

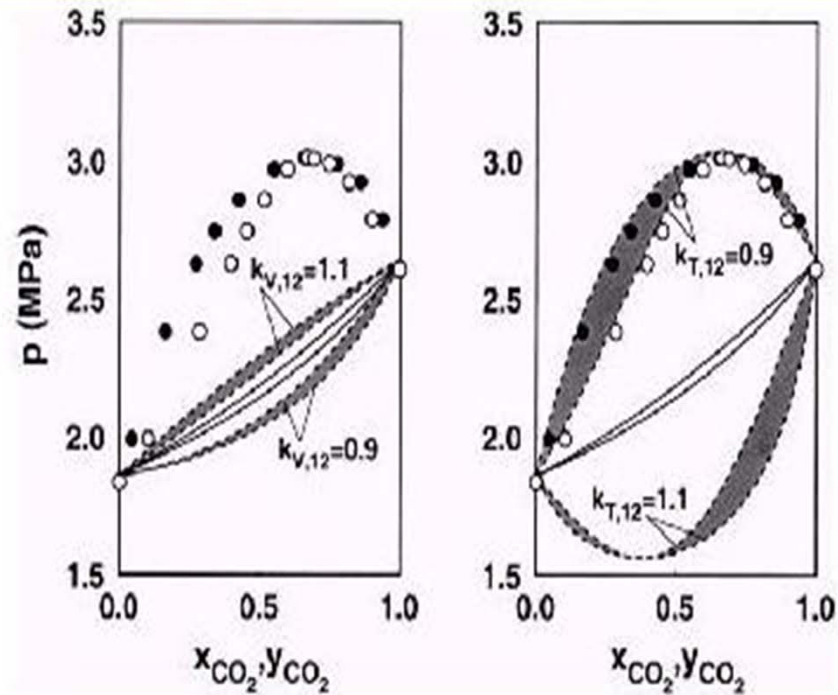


Fig. 4. Influence of the parameters $k_{T,12}$ and $k_{V,12}$ in the quadratic reducing function on the VLE of ethane+carbon dioxide: ○, ● Fredenslund and Mollerup [3]; solid line: $k_T = 1.0$, $k_V = 1.0$.

Enhancement to the Mixture Model

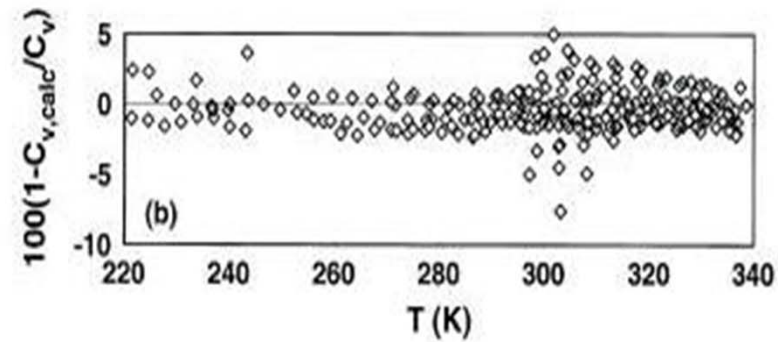


Fig. 5. Deviations between ethane+carbon dioxide isochoric heat capacities and values calculated from the Helmholtz energy model with $k_{T,12} = 0.9$: \diamond Magee [13].

Enhancement to the Mixture Model

- Modification by Tilner-Roth

- ▶ supplement the quadratic expression with β_T, β_V

$$T_n(\mathbf{x}) = x_1^2 T_{n,1} + x_2^2 T_{n,2} + 2x_2(1 - x_2^{\beta_T}) T_{n,12}$$

$$V_n(\mathbf{x}) = x_1^2 V_{n,1} + x_2^2 V_{n,2} + 2x_2(1 - x_2^{\beta_V}) V_{n,12}$$

- ▶ effect of exponents on the shape (Fig.6)
- ▶ influence of $T_{n,12}$ or $V_{n,12}$
 - asymmetric with respect to composition
- ▶ Additional flexibility for tuning of the mixture model

Enhancement to the Mixture Model

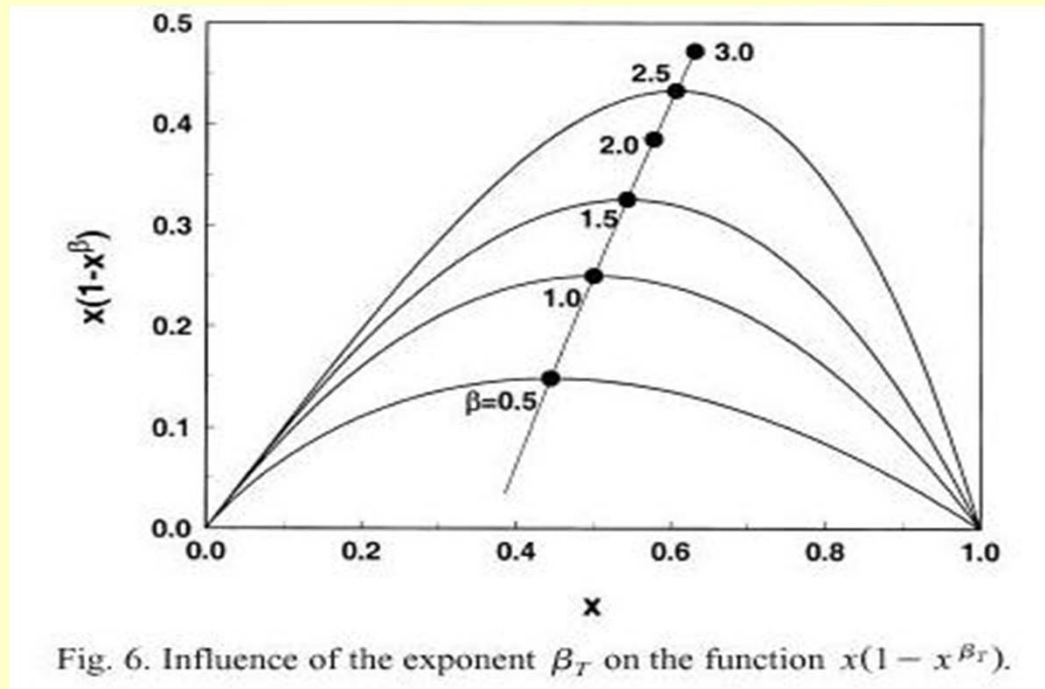


Fig. 6. Influence of the exponent β_T on the function $x(1-x^{\beta_T})$.

Enhancement to the Mixture Model

- Modification by Lemmon

- ▶ modified the linear reducing function

$$T_n(\mathbf{x}) = \sum_{i=1}^l x_i T_{n,i} + \sum_{i=1}^{l-1} \sum_{j=i+1}^l x_i^{\beta_{ij}} x_j \zeta_{ij}$$

$$V_n(\mathbf{x}) = \sum_{i=1}^l x_i V_{n,i} + \sum_{i=1}^{l-1} \sum_{j=i+1}^l x_i x_j \xi_{ij}$$

- ▶ $\zeta_{ij}, \xi_{ij}, \beta_{ij}$: modify the shape of the reducing parameter

- ▶ $\beta_{ij}=1, \quad \zeta_{ij} = (T_{n,i} + T_{n,j})(k_{T,ij} - 1)$

$$\xi_{ij} = (V_{n,i} + V_{n,j})(k_{V,ij} - 1)$$

→ for ethane+CO₂, $\zeta_{ij}=-67.4\text{K}$ ($k_{T,ij}=0.89$)

Departure function

- Departure function

$$\Delta\alpha^r(\tau, \delta, \mathbf{x}) = \sum_{i=1}^{l-1} \sum_{j=i+1}^l x_i x_j \Delta\alpha_{ij}(\tau, \delta, x_i, x_j)$$

- ▶ only to mixture properties, no effect at the pure fluid limits
- ▶ magnitude of departure function
 - generally one order smaller than the residual α^r
- ▶ modeling : regression analysis by Wagner
 - a set of experimental data → lowest standard deviation → bank of terms → subset of term for $\Delta\alpha_{ij}$
 - optimization : modified Marquardt-Fletcher algorithm

Applications by Tillner-Roth

- Introduction an exponent γ in the departure function for a binary system

$$\Delta\alpha^r(\tau, \delta, x) = x_2(1 - x_2^\gamma)\Delta\alpha_{ij}(\tau, \delta, x_i, x_j)$$

- asymmetric influence
 - very effective for simple system, R-152+R134a
 - reduce the number of terms in the departure function
 - applied only to binary systems to date
- ▶ For water+ammonia,

$$x\delta^{n_k}\tau^{m_k}\exp(-\delta^{e_k}) \text{ and } x^2\delta^{n_k}\tau^{m_k}\exp(-\delta^{e_k})$$

Applications by Tillner-Roth

- Results for R-134a+R-32

- ▶ five-term departure function

$$\Delta\alpha^r(\tau, \delta, \mathbf{x}) = x(1-x^\gamma) \left[\sum_{k=1}^2 c_k \delta^{n_k} \tau^{m_k} + \sum_{k=3}^5 c_k \delta^{n_k} \tau^{m_k} \exp(-\delta^{e_k}) \right]$$

- ▶ Fig.7 (cf. Fig.2b)

- density at liquid & vapor region : $\pm 0.1\%$

- density at critical region : $-6 \sim \pm 0.4\%$

Applications by Tillner-Roth

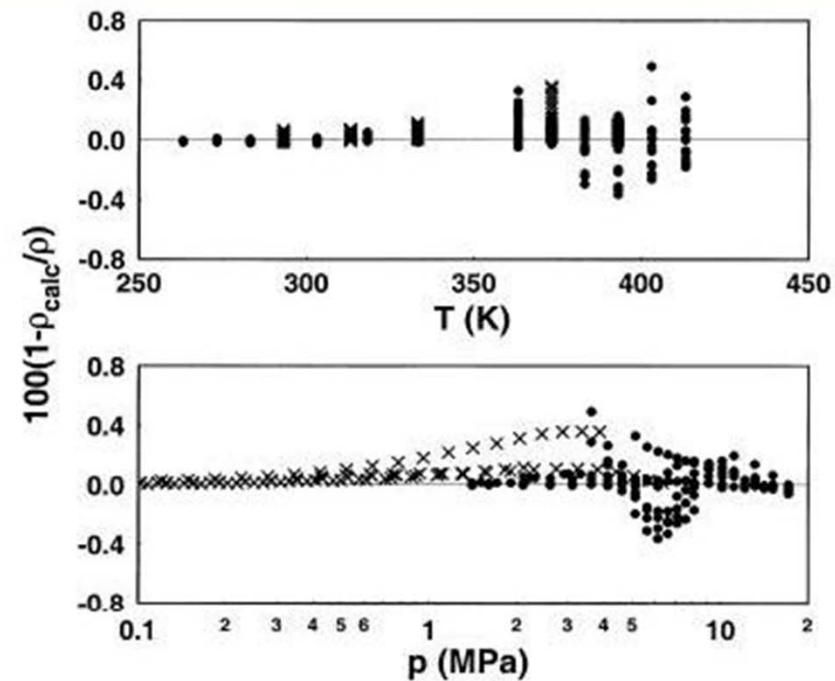


Fig. 7. Deviations between densities of R-134a+R-32 and values calculated from the Helmholtz energy model ($x \approx 0.5$):
● liquid densities of Kleemiss [9]; × vapor densities of Kleemiss [9].

Applications by Tillner-Roth

- Results for water+ammonia

- ▶ 14-term departure function : 19 adjustable parameters

$$\frac{\Delta\alpha^r(\tau, \delta, \mathbf{x})}{x(1-x^\gamma)} = c_1 \delta^{n_1} \tau^{m_1} + \sum_{k=2}^6 c_k \delta^{n_k} \tau^{m_k} \exp(-\delta^{e_k}) + x \sum_{k=7}^{13} c_k \delta^{n_k} \tau^{m_k} \exp(-\delta^{e_k}) \\ + c_{14} x^2 \delta^{n_{14}} \tau^{m_{14}} \exp(-\delta^{e_{14}})$$

- ▶ Fig.8 (cf. Fig.1b, Fig.3c)
 - improved representation

Applications by Tillner-Roth

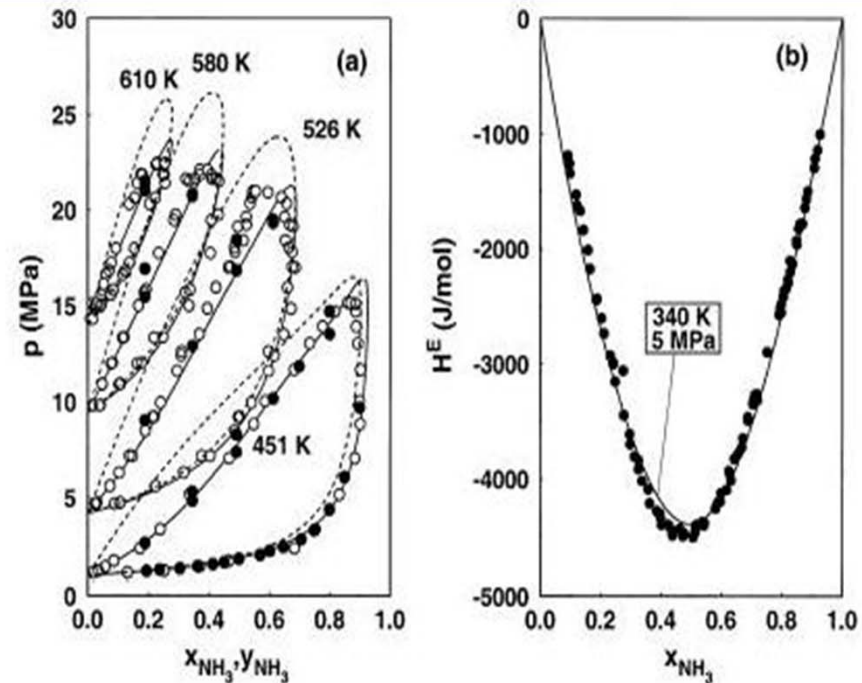


Fig. 8. Vapor-liquid equilibrium and excess enthalpy of water+ammonia. (a) VLE data: \circ Rizvi and Heidemann [21]; \circ Sassen et al. [24]. (b) Excess enthalpies ($298 < T$ (K) < 373 , $5 < p$ (MPa) < 12): \bullet Staudt [28]; solid line: Helmholtz energy model including departure function; dashed line: linear mixture model.

Applications by Lemmon

- Generalized departure function

$$\Delta\alpha^r(\tau, \delta, \mathbf{x}) = \sum_{i=1}^{l-1} \sum_{j=i+1}^l x_i x_j F_{ij} \Delta\alpha_{ij}(\tau, \delta)$$

$$\Delta\alpha_{ij}(\tau, \delta) = \sum_{k=1}^{10} c_k \delta^{n_k} \tau^{m_k}$$

- ▶ c_k, n_k, m_k : fixed the same for all mixture
- ▶ $F_{ij}, \zeta_{ij}, \xi_{ij}, \beta_{ij}$: adjustable parameters from (p, V, T, x)
 - 0.2% in density, 1% in heat capacities
 - 1-2% bubble point pressure at critical temp.
 - 5-10% bubble point pressure at critical temp. father apart

Applications by Lemmon

- Results

- ▶ propane + *n*-butane : Fig.10
 - less than 0.04% average absolute deviation in density
 - 0.4% average absolute deviation in bubble point pressure
- ▶ Uncertainty of the equation reported
 - 0.2% in density
 - 1% in heat capacities
- ▶ Fig.11 : ternary refrigerant mixture

Applications by Lemmon

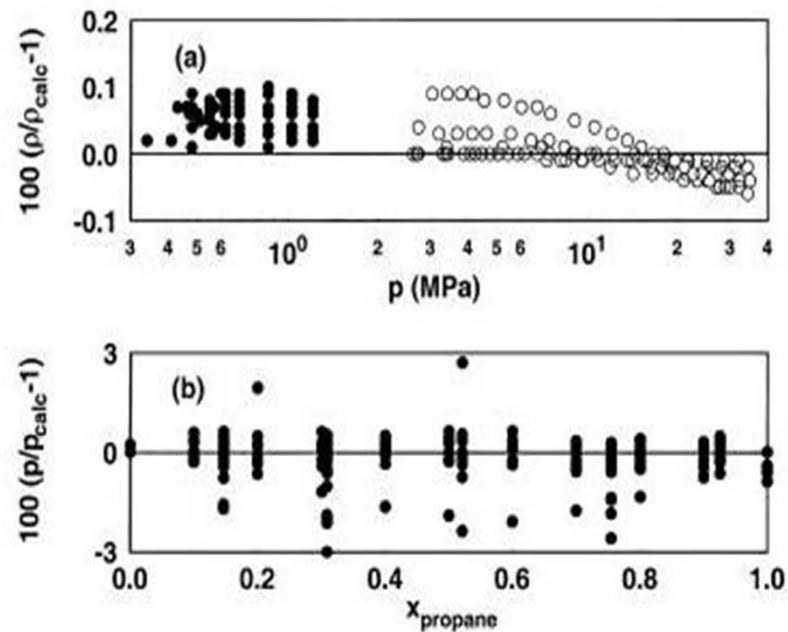


Fig. 10. The mixture propane + *n*-butane. (a) Deviations between liquid densities and values predicted from the Helmholtz energy model: ● Parrish [16] ($283 < T$ (K) < 333 , $0.15 < x_{\text{propane}} < 0.75$); ○ Magee [14] ($244 < T$ (K) < 400 , $x_{\text{propane}} \approx 0.6$). (b) Deviations between bubble point pressures and values predicted from the Helmholtz energy model: ● Kay [8] ($332 < T$ (K) < 425).

Applications by Lemmon

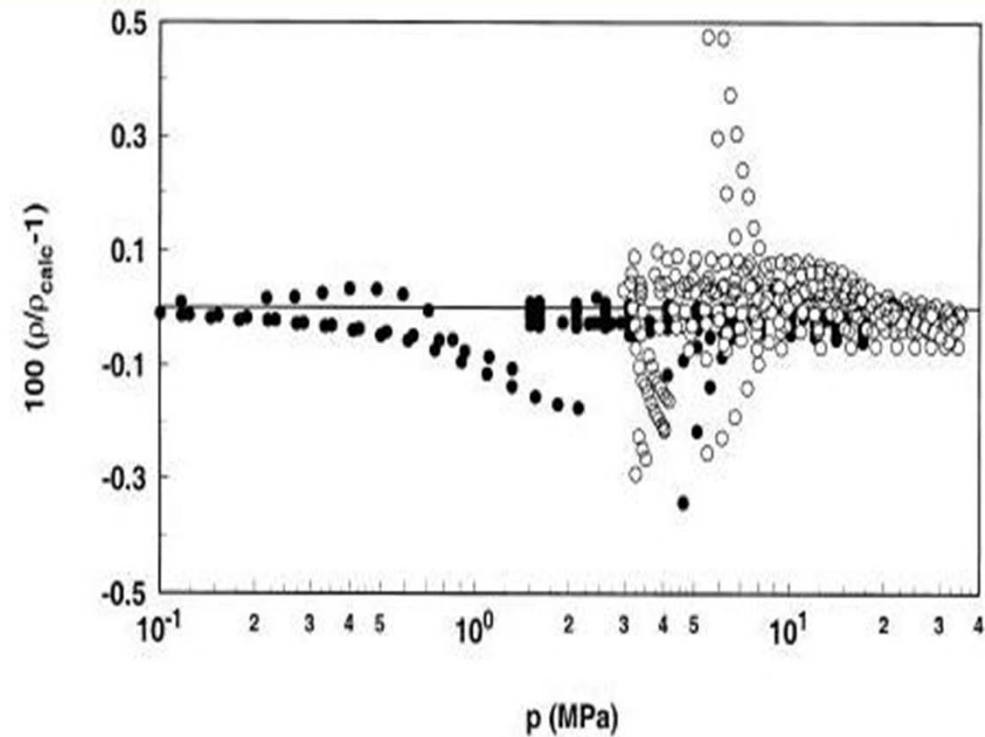


Fig. 11. Deviations between experimental densities for the ternary system R-134a + R-125 + R-32 and values predicted from the Helmholtz energy model: ● Kleemiss [9] ($243 < T$ (K) < 353); ○ Magee and Haynes [15] ($200 < T$ (K) < 400).

Conclusions

- EOS for mixture in terms of the Helmholtz energy has been developed and applied to several fluid systems by two different research groups
- By Tillner-Roth, model of single binary systems for which comprehensive accurate data are available
- By Lemmon, generalized model was presented which accurately predicts thermodynamic properties of mixtures
- Further research for more nonideal systems and complex multicomponent mixtures