

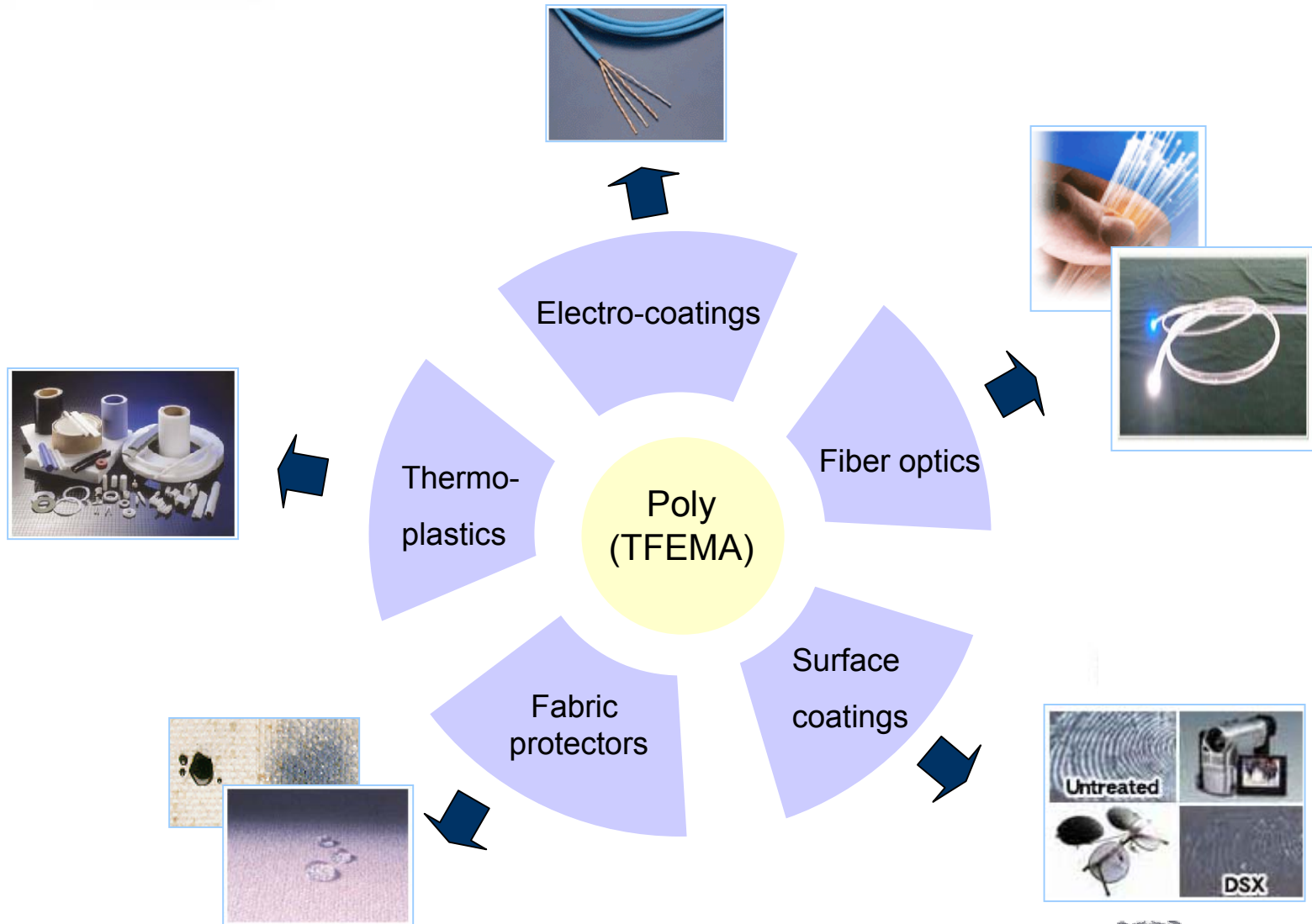
# Phase behavior and modeling of CO<sub>2</sub> + 2,2,2-trifluoroethyl methacrylate and CO<sub>2</sub> + poly (2,2,2-trifluoroethyl methacrylate) systems

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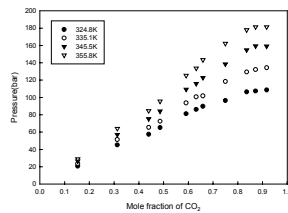
# Objectives — Applications of poly (TFEMA)



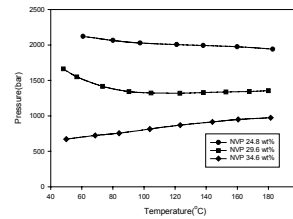
# Objectives — 초임계 상거동 자료의 용도 예

초임계 유체를 이용한  
고분자 합성

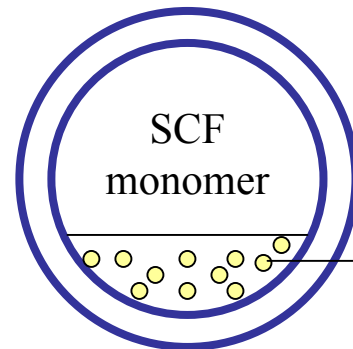
Binary mixture of  
CO<sub>2</sub>+monomer or polymer



Ternary mixture of Polymer  
+ monomer + CO<sub>2</sub>



Initial State



Final State

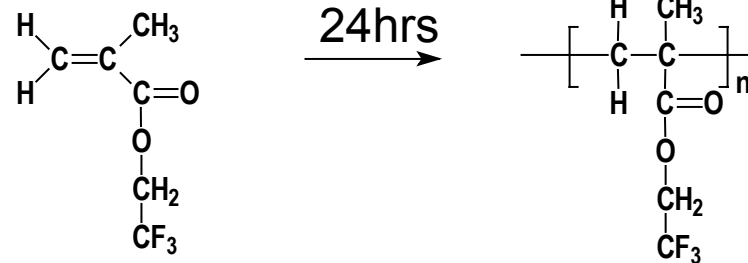
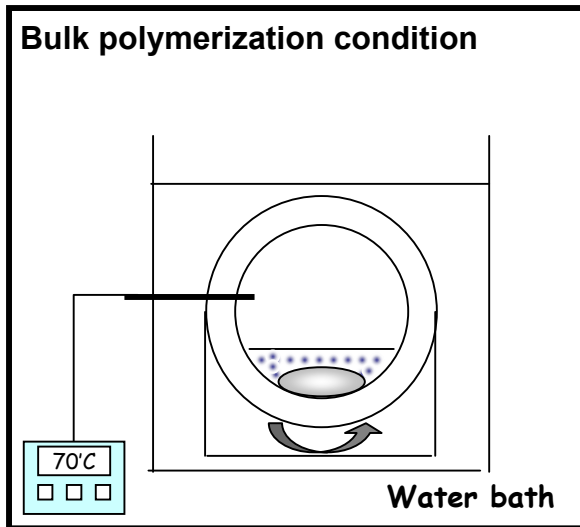
Polymer

• 최적 중합조건 결정

• 중합 후 잔류 단량체 제거

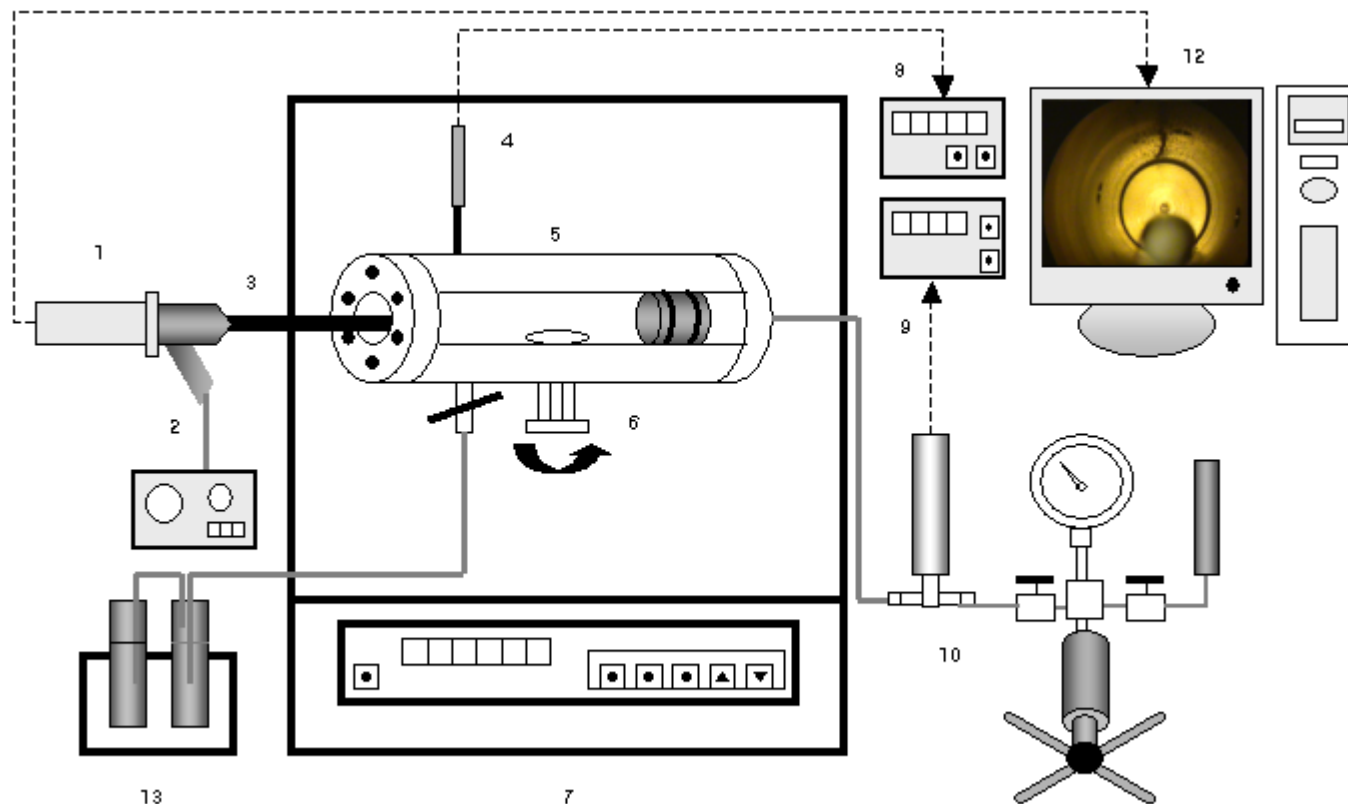
# Materials

- Carbon dioxide (min. 99.99% purity) - Korea industrial Gases
- 2,2,2-trifluoroethyl methacrylate: (TFEMA: min. 99% purity) - Aldrich
- poly (2,2,2-trifluoroethyl methacrylate): bulk polymerization



- Initiator ; AIBN [1.0 wt% of monomer]
- Temperature ;  $70 \pm 0.5^\circ\text{C}$
- $\bar{M}_w$  ; 268,000 PDI ; 1.6
- characterization by GPC

# Experimental apparatus – variable volume cell



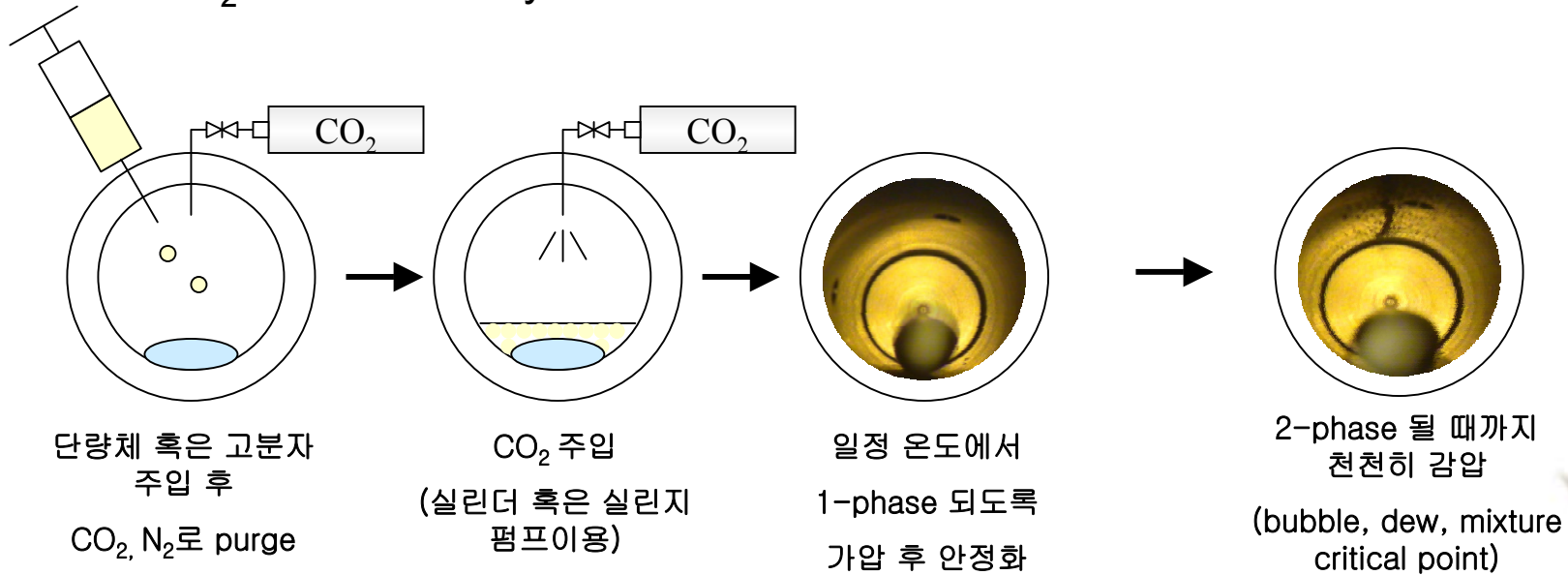
1. Camera
2. Light source
3. Borescope
4. Thermocouple

5. View cell
6. Magnetic stirrer
7. Air bath
8. Digital thermometer

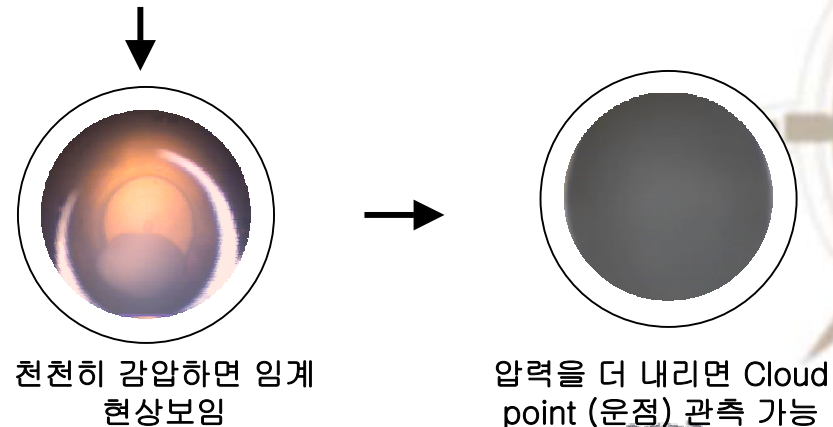
9. Digital pressure transducer
10. Pressure gauge
11. Hand pump
12. Computer monitor
13. Trap

# Experimental procedure

## ➤ CO<sub>2</sub> + monomer system



## ➤ CO<sub>2</sub> + polymer system



# Calculation: Peng-Robinson equation of state

## ➤ Peng-Robinson EOS

$$P = \frac{RT}{V - b} - \frac{a \alpha}{V^2 + 2bV - b^2}$$

$$a = 0.45724 R^2 T_c^2 / P_c$$

$$b = 0.07780 R T_c / P_c$$

$$\alpha = [1 + (0.37464 + 1.54226 \omega - 0.26992 \omega^2)(1 - T_r^{0.5})]^2$$

pure parameters

→  $T_c, P_c, \omega$

## ➤ van der Waals 1-fluid mixing rule

$$a_{mix} = \sum_i \sum_j x_i x_j a_{ij}$$

$$a_{ij} = \sqrt{(a_{ii} a_{jj})} (1 - k_{ij})$$

$$b_{mix} = \sum_i \sum_j x_i x_j b_{ij}$$

$$b_{ij} = \frac{(b_{ii} + b_{jj})}{2}$$

binary parameter

→  $k_{ij}$

$$OBF = \sum_i^N \left( \frac{P_{exp} - P_{cal}}{P_{exp}} \right)^2$$

# Calculation: Sanchez-Lacombe lattice-fluid equation of state

$$\tilde{\rho}^2 + \tilde{P} + \tilde{T} \left[ \ln(1 - \tilde{\rho}) + \left(1 - \frac{1}{r}\right) \tilde{\rho} \right] = 0$$

$$\text{or } \frac{\tilde{P}\tilde{v}}{\tilde{T}} = \frac{1}{r} - \left[ 1 + \tilde{v} \ln \left( 1 - \frac{1}{\tilde{v}} \right) \right] - \frac{1}{\tilde{v}\tilde{T}}$$

$$\tilde{T} \equiv \frac{T}{T^*}$$

$$T^* = \frac{\varepsilon^*}{k}$$

$$\tilde{P} \equiv \frac{P}{P^*}$$

$$P^* = \frac{\varepsilon^*}{v^*}$$

$$\tilde{v} \equiv \frac{1}{\tilde{\rho}} \equiv \frac{V}{V^*} \equiv \frac{\rho^*}{\rho}$$

$$V^* = N(rv^*)$$

pure parameters

$$T^*, P^*, \rho^*$$

or

$$\varepsilon^*, v^*, r$$

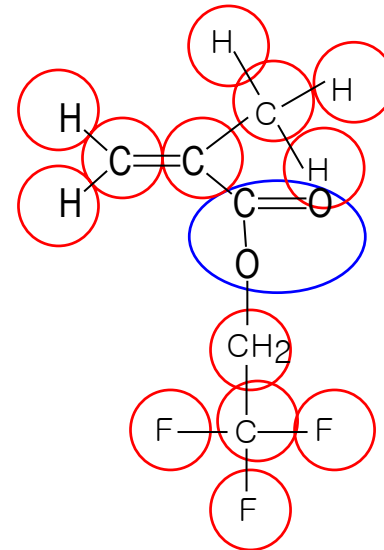


# Estimation method of pure parameters : TFEMA

## ➤ **Group Contribution method**

### **: Method of Wilson and Japerson**

Critical constants  $T_c$ ,  $P_c$ , Estimation based Zero, first and second order methods (1996)



$$T_b = 380.15\text{K} \quad \text{F-Tech Inc. data}$$

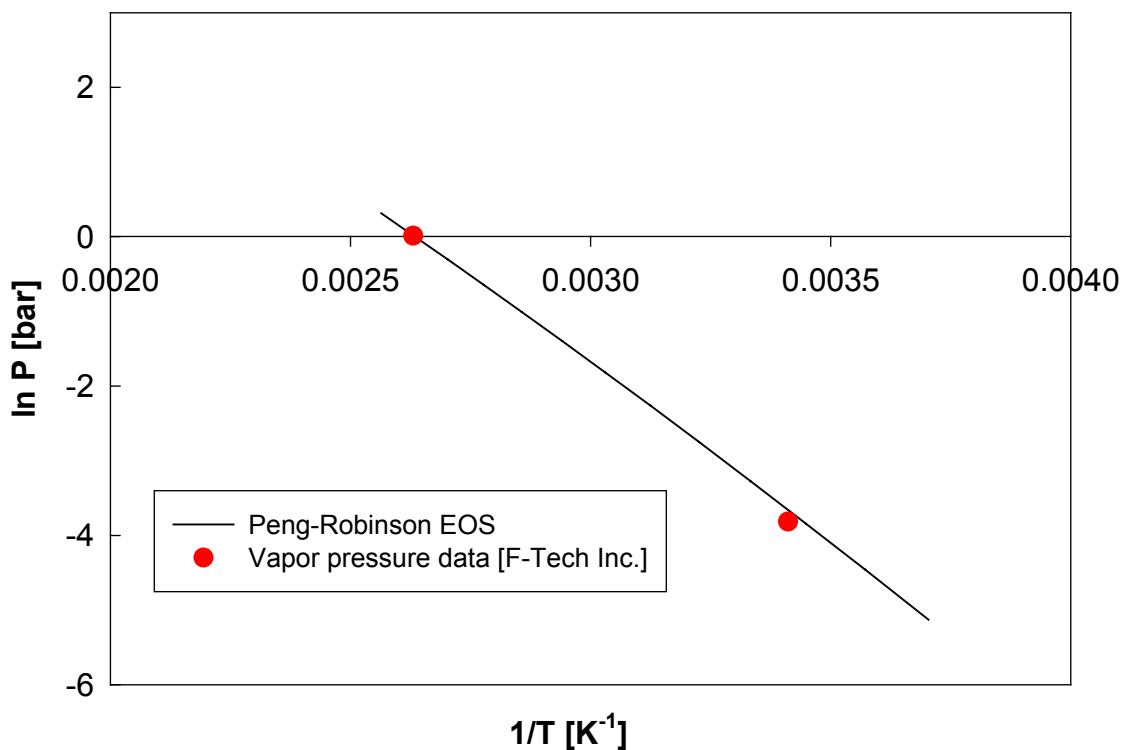
$$T_c = T_b / [(0.048271 - 0.019846 N_r + \sum_k N_k (\Delta tck) + \sum_j M_j (\Delta tcj) + ]^{0.2}$$

$$P_c = 0.0186233 T_c / [-0.96601 + \exp(Y)]$$

$$Y = -0.00922295 - 0.0290403 N_r + 0.041 \left( \sum_k N_k (\Delta pck) + \sum_j M_j (\Delta pcj) \right)$$

# Estimation method of pure parameters : TFEMA

	Unit	TFEMA
$T_b$	K	380.15
$T_c$	K	541.12
$P_c$	bar	29.13
$\omega$	-	0.4773



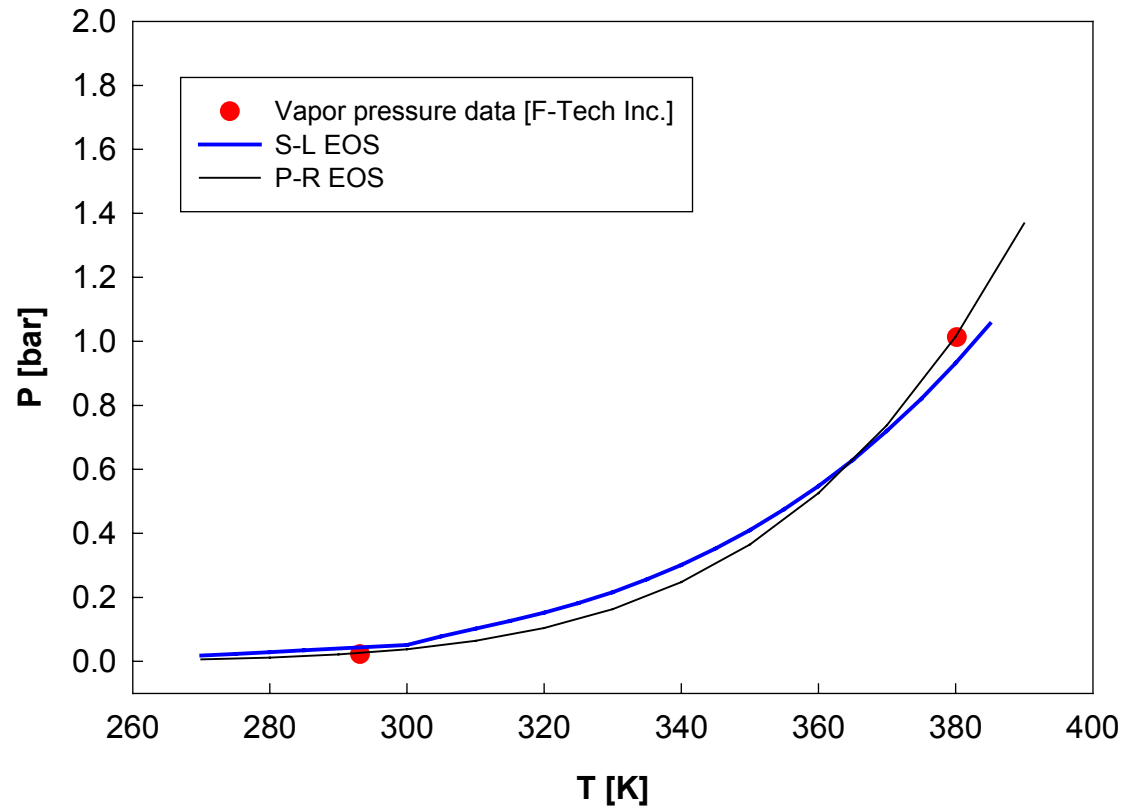
$\omega$  : Lee-Kesler method

→ Vapor pressure data 이용하여 S-L parameters 구함

# Estimation method of pure parameters : TFEMA

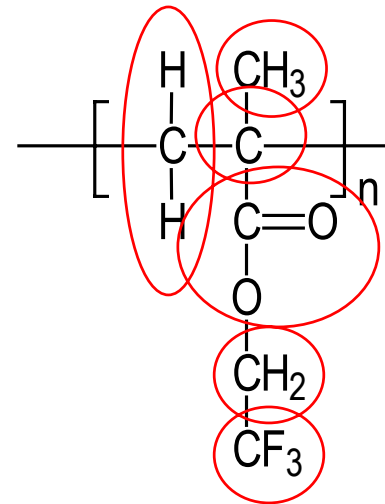
	Unit	TFEMA	CO <sub>2</sub>
T*	K	711.40	305.00
P*	MPa	294.79	574.50
$\rho^*$	kg/m <sup>3</sup>	1167.20	1510.00

CO<sub>2</sub> parameter : Journal of Applied Polymer Science, Vol. 36, 583-597 (1988)



# Estimation method of pure parameters : poly (TFEMA)

First order	n	T*	P*	$\rho^*$
CH <sub>3</sub>	1	-18.08	-105.41	-100.69
CH <sub>2</sub>	2	-7.65	-29.67	-46.65
C	1	97.41	82.23	136.60
COO	1	-76.38	168.96	363.43
CF <sub>3</sub>	1	-54.57	-134.86	67.12



$$f(X) = X - X_0 \quad (X = T^*, P^* \text{ or } \rho^*)$$

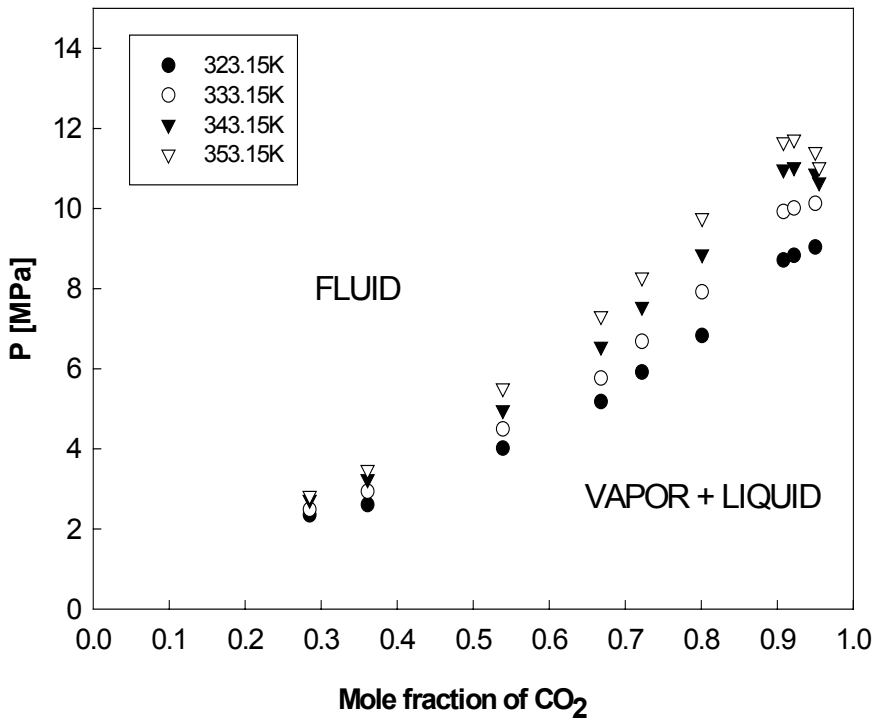
parameter	value
T <sub>o</sub> *	666.95 K
P <sub>o</sub> *	489.46 MPa
$\rho^*_o$	1019.47 kg/m <sup>3</sup>

	Unit	Poly(TFEMA)	CO <sub>2</sub>
T*	K	600.03	305.00
P*	MPa	441.04	574.50
$\rho^*$	kg/m <sup>3</sup>	1392.63	1510.00

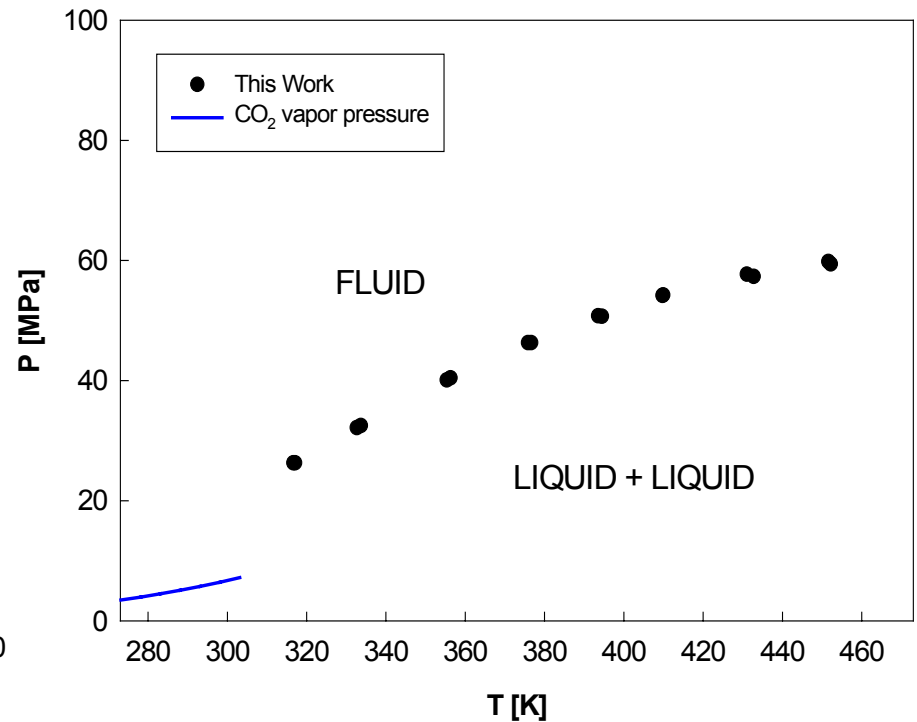
Ing. Eng. Chem. Res., Vol. 36, 3968-3973 (1997)

# Experimental Results

Pressure-composition (P-x) isotherms

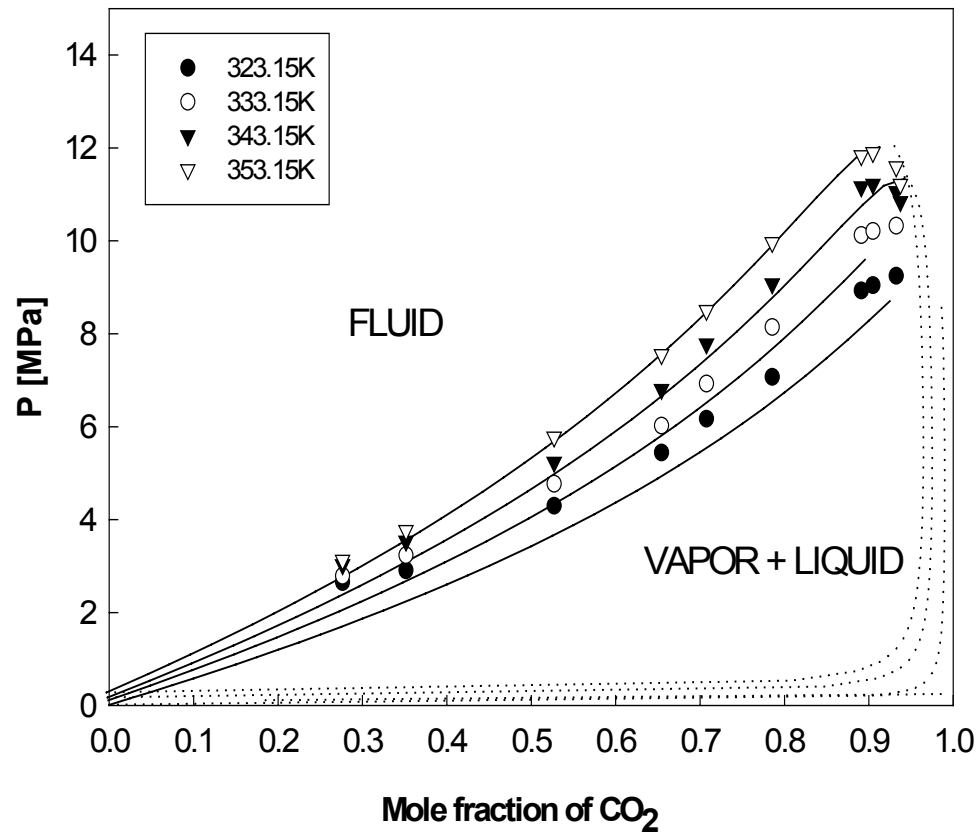


Temperature-Pressure (T-P) diagram of CO<sub>2</sub> + poly (TFEMA) system: LCST behavior



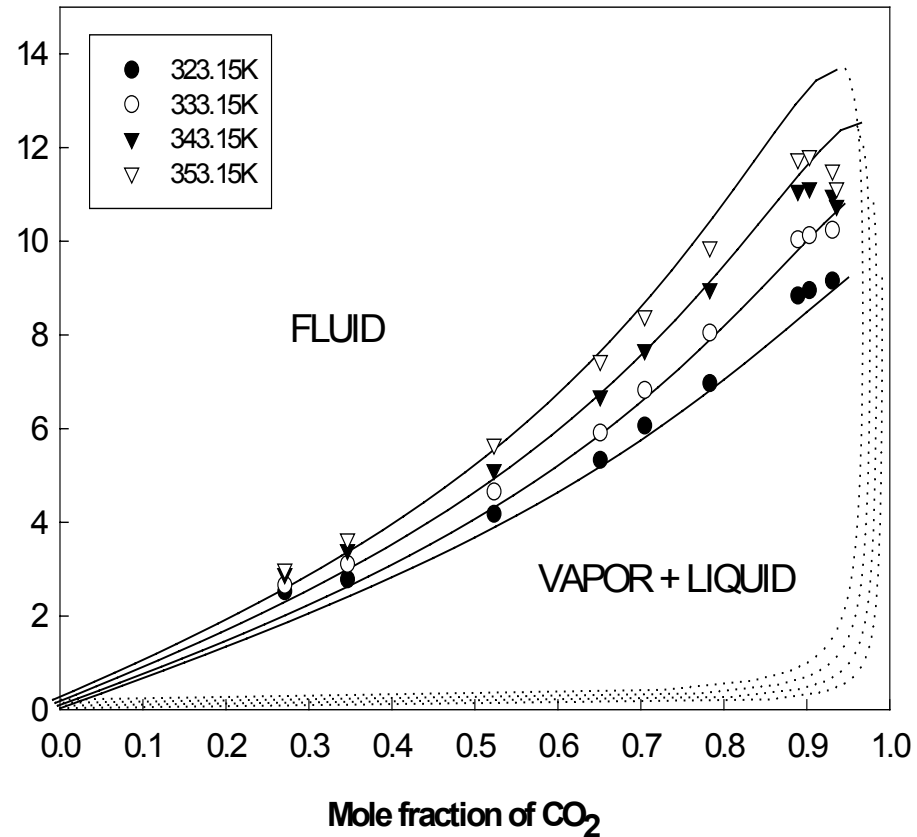
# Modeling 1 – CO<sub>2</sub> + TFEMA system

## Peng-Robinson EOS



$k_{ij}$	-0.0126
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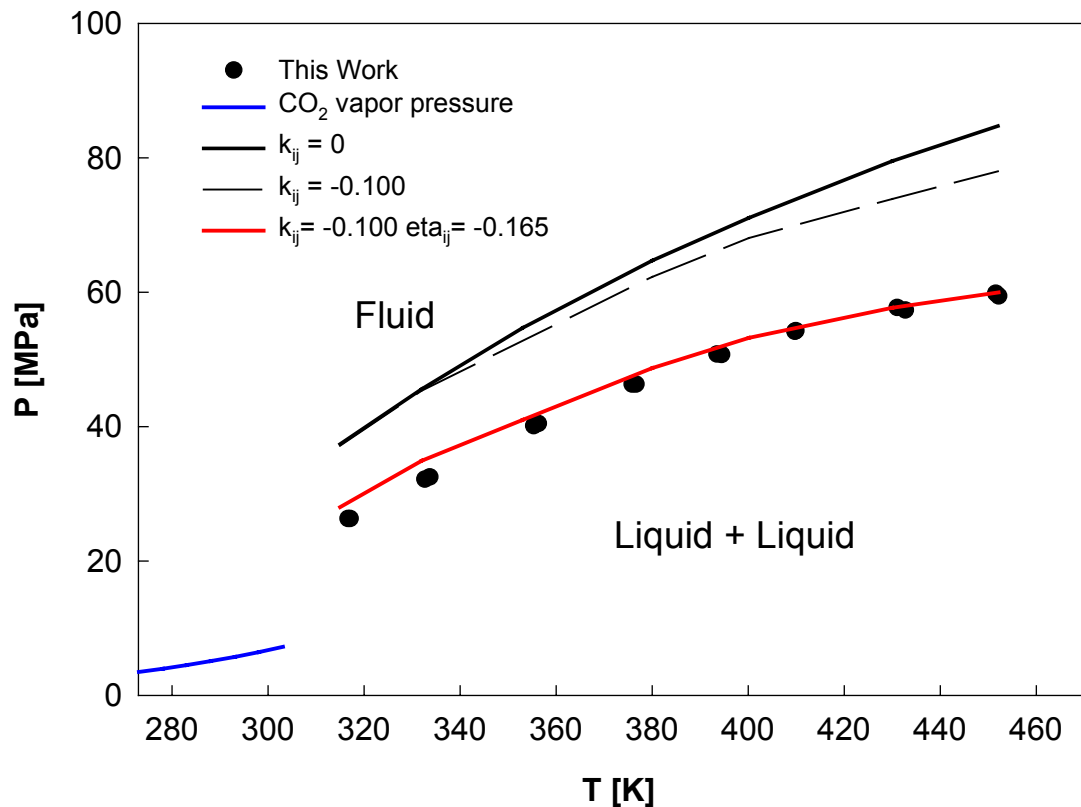
## Sanchez-Lacombe lattice-fluid EOS



T [K]	323.15	333.15	343.15	353.15
$k_{ij}$	0.1159	0.1010	0.0933	0.0847

# Modeling 3 – CO<sub>2</sub> + poly (TFEMA) system

P-T diagram : Sanchez-Lacombe lattice-fluid EOS  
 Lower Critical Solution Temperature



Poly (TFEMA) : 3.91wt%

# Conclusions

- 온도 323.15 ~ 353.15K, 압력 20~120 bar 범위에서 CO<sub>2</sub> + trifluoroethyl methacrylate 계에 대한 고압 상평형 데이터(P-x diagram)를 variable volume view cell을 이용하여 얻었다.
- 온도 320 ~ 460 K, 압력 320~600 bar 범위에서 CO<sub>2</sub> + poly (trifluoroethyl methacrylate) 계에 관한 임계 거동(LCST critical locus)을 관측하였다.
- CO<sub>2</sub>와 TFEMA, poly (TFEMA)의 상거동에 대하여 pure parameters를 그룹기여 방법을 이용하여 얻고 P-R EOS와 S-L EOS로 모델링 하였다.  
CO<sub>2</sub> + trifluoroethyl methacrylate 계의 경우 S-L EOS가 임계점을 높게 예측하는 것을 알 수 있었다. CO<sub>2</sub> + poly (trifluoroethyl methacrylate) 계는 두개의 binary parameters를 이용하여 모델링 하였다.
- 앞으로 CO<sub>2</sub> + poly (trifluoroethyl methacrylate) + trifluoroethyl methacrylate에 관한 ternary phase behavior에 관한 실험 및 모델링을 연구해보고자 한다.