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(54) Title: NOVEL CARBON FIBRILS, METHOD FOR PRODUCING SAME, AND COMPOSITIONS CONTAINING SAME		
(57) Abstract A discrete carbon fibril characterized by a substantially constant diameter between about 3.5 and about 70 nanometers, length greater than about 5 times the diameter and less than about 100 times the diameter, an outer region of multiple essentially continuous layers of ordered carbon atoms and a distinct inner core region. The invention further concerns a plurality of such fibrils. The fibrils of this invention may be produced by contacting for an appropriate period of time and at a suitable pressure a suitable metal-containing particle with a suitable gaseous, carbon-containing compound, at a temperature between about 850°C and 1200°C, or by treating discrete carbon fibrils, characterized by a length greater than about 100 times the diameter. Carbon fibrils may also be continuously produced by continuously contacting for an appropriate period of time at suitable conditions. Another aspect of the invention concerns a composition of matter comprising a carbon fiber or a carbon plate and a plurality of fibrils. Carbon fibrils and compositions of matter comprising carbon fibrils are useful in composites having a matrix of e.g., an organic polymer, an inorganic polymer or a metal. In specific embodiments, the fibrils or the compositions of matter may be used to reinforce a structural material, to enhance the electrical or thermal conductivity of a material, to increase the surface area of an electrode or capacitor plate, to provide a support for a catalyst, or to shield an object from electromagnetic radiation.		

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NOVEL CARBON FIBRILS, METHOD FOR PRODUCING SAME, AND
COMPOSITIONS CONTAINING SAME

BACKGROUND OF THE INVENTION

This application is a continuation-in-part of U.S. Serial No. 678,701, filed December 6, 1984, the contents of which are hereby incorporated by reference into the present application.

This invention relates to the production of graphitic carbon fibrils having high surface area, high Young's modulus of elasticity and high tensile strength. More specifically, it relates to such fibrils grown catalytically from inexpensive, readily available carbon precursors without the need for usual and expensive graphitizing temperatures (approximately 2900°C).

Fiber-reinforced composite materials are becoming increasingly important because their mechanical properties, notably strength, stiffness and toughness, are superior to the properties of their separate components or of other non-composite materials. Composites made from carbon fibers excel in strength and stiffness per unit weight, hence they are finding rapid acceptance in aerospace and sporting goods applications. Their high cost, however, inhibits wider use.

Carbon fibers are currently made by controlled pyrolysis of continuous filaments of precursor organic polymers, notably cellulose or polyacrylonitrile, under carefully maintained tension, which is needed to insure proper orientation of the anisotropic sheets of carbon atoms in the final filaments. Their high cost is a consequence of the cost of the preformed organic fi-

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bers, the weight loss in carbonization, the slow rate of carbonization in expensive equipment and the careful handling necessary to avoid breaks in the continuous filaments.

There has been intense development of methods of spinning and carbonizing hydrocarbon pitch fiber to reduce precursor filament cost and weight loss. So far, the pitch pre-treatment, spinning conditions and post-treatments needed to insure correct orientation of the sheets of carbon atoms in the final products have been nearly as expensive as the previously noted method involving organic polymers. Both methods require use of continuous filaments to achieve high orientation and, thereby, optimum properties. There is a practical lower limit of fiber diameter, i.e., 6 to 8 micrometers, below which fiber breakage in spinning and post-treatments becomes excessive.

An entirely distinct approach to carbon fiber formation involves the preparation of carbon filaments through the catalytic decomposition at metal surfaces of a variety of carbon-containing gases, e.g., CO/H₂, hydrocarbons, and acetone. These filaments are found in a wide variety of morphologies (e.g., straight, twisted, helical, branched) and diameters (e.g., ranging from tens of angstroms to tens of microns). Usually, a mixture of filament morphologies is obtained, frequently admixed with other, non-filamentous carbon (cf. Baker and Harris, Chemistry and Physics of Carbon, Vol. 14, 1978). Frequently, the originally formed carbon filaments are coated with poorly organized thermal carbon. Only relatively straight filaments possessing relatively large graphitic domains oriented with their c-axes perpendicular to the fiber axis and possessing

little or no thermal carbon overcoat will impart the properties of high strength and modulus required in reinforcement applications.

Most reports that cite formation of filamentous carbon do not document the particular type of filaments formed, so that it is impossible to determine whether the filaments are suitable for reinforcement applications. For example, Baker et al., in British Patent 1,499,930 (1977), disclose that carbon filaments are formed when an acetylene or diolefin is decomposed over catalyst particles at 675-775°C. No description of the structure of these filaments is given, however. In European Patent Application EP 56,004 (1982), Tates and Baker describe the formation of filamentous carbon over FeO_x substrates, but again do not disclose any information concerning the structure of the carbon filaments formed. Bennett et al., in United Kingdom Atomic Energy Authority Report AERE-R7407, describe the formation of filamentous carbon from catalytic decomposition of acetone, but also fail to give any indication of the morphology, and hence suitability for reinforcement applications, of the carbon formed.

Several groups of workers have disclosed the formation of straight carbon filaments through catalytic decomposition of hydrocarbons. Oberlin, Endo, and Koyama have reported that aromatic hydrocarbons such as benzene are converted to carbon fibers with metal catalyst particles at temperatures of around 1100°C, Carbon 14:133 (1976). The carbon filaments contain a well ordered, graphitic core of approximately the diameter of a catalyst particle, surrounded by an overcoat of less organized thermal carbon. Final filament diameters are in the range of 0.1 to 80 microns. The authors infer that

the graphitic core grows rapidly and catalytically, and that thermal carbon subsequently deposits on it, but state that the two processes cannot be separated "because they are statistically concomitant." *Journal of Crystal Growth* 32:335 (1976). The native fibers, coated with thermal carbon, possess low strength and stiffness, and are not useful as a reinforcing filler in composites. An additional high temperature treatment at 2500-3000°C is necessary to convert the entire filament to highly ordered graphitic carbon. While this procedure may be an improvement on the difficult and costly pyrolysis of preformed organic fibers under tension, it suffers from the drawback that a two step process of fiber growth and high temperature graphitization is required. In addition, the authors state nothing regarding deliberate catalyst preparation, and catalyst particles appear to be adventitious. In more recent work, preparation of catalytic particles is explored, but the two processes of catalytic core growth and thermal carbon deposition are again not separated, *Extended Abstracts, 16th Biennial Conference on Carbon: 523* (1983).

Tibbetts has described the formation of straight carbon fibers through pyrolysis of natural gas in type 304 stainless steel tubing at temperatures of 950-1075°C, *Appl. Phys. Lett.* 42(8):666 (1983). The fibers are reported to grow in two stages similar to those seen by Koyama and Endo, where the fibers first lengthen catalytically and then thicken by pyrolytic deposition of carbon. Tibbetts states that these stages are "overlapping", and he is unable to grow filaments free of pyrolytically deposited carbon. In addition, Tibbetts's approach is commercially impractical for at least two reasons. First, initiation of fiber growth

occurs only after slow carbonization of the steel tube (typically about ten hours), leading to a low overall rate of fiber production. Second, the reaction tube is consumed in the fiber forming process, making commercial scale-up difficult and expensive.

It has now unexpectedly been found that it is possible to catalytically convert hydrocarbon precursors to carbon filaments substantially free of pyrolytically deposited thermal carbon, and thereby to avoid the thickening stage reported in the prior art as "overlapping" and "concomitant" with the filament lengthening stage. This ability allows the direct formation of high strength fibrils useful in the reinforcement of matrices, in the preparation of electrode materials of very high surface area, and in the shielding of objects from electromagnetic radiation.

SUMMARY OF THE INVENTION

This invention concerns an essentially cylindrical discrete carbon fibril characterized by a substantially constant diameter between about 3.5 and about 70 nanometers, e.g. between about 7 and 25 nanometers, length greater than about 5 times the diameter and less than about 100 times the diameter, an outer region of multiple essentially continuous layers of ordered carbon atoms and a distinct inner core region, each of the layers and the core being disposed substantially concentrically about the cylindrical axis of the fibril. Preferably the entire fibril is substantially free of thermal carbon overcoat.

The inner core of the fibril may be hollow or may contain carbon atoms which are less ordered than the ordered carbon atoms of the outer region, which are graphitic in nature.

The fibril of this invention may be produced by treating an essentially cylindrical discrete carbon fibril, characterized by a substantially constant diameter between about 3.5 and about 70 nanometers, length greater than about 10^2 times the diameter, an outer region of multiple essentially continuous layers of ordered carbon atoms and a distinct inner core region, each of the layers and the core being disposed substantially concentrically about the cylindrical axis of the fibril, so as to produce the carbon fibril.

The fibril of this invention may also be produced by contacting for an appropriate period of time and at a suitable pressure a suitable metal-containing particle with a suitable gaseous, carbon-containing compound, at

a temperature between about 850°C and about 1200°C, the ratio on a dry weight basis of carbon-containing compound to metal-containing particle being at least about 100:1.

A carbon fibril may also be continuously produced by continuously contacting for an appropriate period of time at a suitable pressure suitable metal-containing particles with a suitable gaseous, carbon-containing compound, at a temperature between about 850°C and about 1200°C, and recovering the fibrils so produced. The fibrils produced by this method may be recovered in association with the metal-containing particles or, alternatively, separated from the metal-containing particles and recovered. The continuous contacting may be effected by continuously introducing the gaseous, carbon-containing compound into a reaction zone containing the metal-containing particles and continuously withdrawing the gaseous carbon-containing compound from the reaction zone, or by continuously introducing the metal-containing particles into a reaction zone containing a defined volume of the gaseous, carbon-containing compound and continuously withdrawing the metal-containing particles from the reaction zone, or by continuously introducing both the metal-containing particles and the gaseous, carbon-containing compound into a reaction zone and continuously withdrawing both from the reaction zone.

In the above-mentioned method for continuously producing carbon fibrils, the withdrawn gaseous, carbon-containing compound or the withdrawn metal-containing particles may be treated so as to remove any undesirable material, i.e. impurities or reaction by-products, and then reintroduced into the reaction zone.

It is further contemplated that a portion of the fibrils in association with the metal-containing particles may be continuously recovered, dispersed with additional metal-containing particles, and continuously reintroduced into contact with the gaseous carbon-containing compound.

The contacting of the metal-containing particle with the carbon-containing compound may be carried out in the presence of a compound, e.g. CO_2 , H_2 or H_2O , capable of reaction with carbon to produce gaseous products.

Suitable carbon-containing compounds include hydrocarbons, including aromatic hydrocarbons, e.g. benzene, toluene, xylene, cumene, ethylbenzene, naphthalene, phenanthrene, anthracene or mixtures thereof; non-aromatic hydrocarbons, e.g., methane, ethane, propane, ethylene, propylene or acetylene or mixtures thereof; and oxygen-containing hydrocarbons, e.g. formaldehyde, acetaldehyde, acetone, methanol, or ethanol or mixtures thereof; and include carbon monoxide.

The suitable metal-containing particle may be a cobalt-, nickel-, or iron-containing particle, including a particle derived from a metal salt that is thermally decomposable at a temperature below about 1200°C , having a diameter between about 3.5 and about 70 nanometers.

Such particles may be supported on a chemically compatible, refractory support, e.g., a support of alumina; carbon, including carbon fibers, carbon fibrils, or carbon plates; or a silicate, including an aluminum silicate.

The suitable metal-containing particle may be encapsulated in carbon or a carbon-containing compound of e.g., a carbide or an organic polymer, including polystyrene and starch.

In one embodiment, the surface of the metal-containing particle is independently heated, e.g. by electromagnetic radiation, to a temperature between about 850°C and about 1800°C, the temperature of the particle being higher than the temperature of the gaseous, carbon-containing compound.

In a specific embodiment, the metal-containing particle is contacted with the carbon-containing compound for a period of time from about 10 seconds to about 30 minutes at a pressure of from about one-tenth atmosphere to about ten atmospheres. In this embodiment, the metal-containing particle is an iron-containing particle, the gaseous carbon-containing compound is carbon monoxide and the reaction temperature is between 900°C and 1150°C. The contacting may be carried out in the presence of gaseous hydrogen. Additionally, the iron-containing particle may be a particle derived from iron oxalate and may be supported on a chemically compatible, refractory support of e.g., carbon.

This invention also concerns a method for producing a substantially uniform plurality of essentially cylindrical, discrete carbon fibrils which comprises contacting for an appropriate period of time and at a suitable pressure, suitable metal-containing particles with a suitable gaseous, carbon-containing compound, at a temperature between about 850°C and about 1200°C. Preferably, each of the fibrils so produced has a diam-

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eter substantially equal to the diameter of each other fibril. In one embodiment the metal-containing particles are pre-formed.

The fibrils are useful in composites having a matrix of e.g., an organic polymer, an inorganic polymer, a metal, an adhesive, or a ceramic material. The fibrils may be dispersed in the matrix, oriented into tows of fibrils which are dispersed in the matrix, or entangled together to form a fibril mat which is disposed in the matrix.

Another aspect of this invention concerns a "furry" fiber, a "furry" plate, or a branched fibril which comprises a carbon fiber, a carbon plate, or a carbon fibril, respectively, and a plurality of carbon fibrils adhering to the outer surface of the fiber, plate, or fibril, respectively. A method for producing furry fibers, furry plates, or branched fibrils comprises dispersing suitable metal-containing particles on the outer surface of a carbon fiber, plate, or fibril, respectively, and contacting with a suitable gaseous, carbon-containing compound for an appropriate period of time and at a suitable pressure. Composites comprising a matrix and furry fibers, furry plates, or branched fibrils may be produced by e.g., dispersion or impregnation.

Carbon fibrils (including tows of fibrils), fibril mats, furry fibers, furry plates or branched fibrils may be used to reinforce a structural material, to enhance the electrical or thermal conductivity of a material, to increase the surface area of an electrode or an electrolytic capacitor plate, to provide a support for a catalyst, or to shield an object from electromagnetic radiation.

This invention also concerns a method for encapsulating a metal-containing catalytic particle in e.g., carbon, a carbon-containing compound, or an organic polymer. The metal-containing particle may be a cobalt-, nickel-, or iron-containing particle, including a particle derived from a metal salt that is thermally decomposable at a temperature below about 1200°C, and may be supported on a chemically compatible, refractory support e.g., a support of alumina, carbon, including a carbon fiber or a carbon fibril, or a silicate.

The method for producing a substantially uniform plurality of encapsulated metal-containing particles comprises treating for an appropriate period of time the metal-containing particles with a carbon-containing compound at a suitable temperature below 800°C. In a specific embodiment, iron oxalate is treated with acetylene for a period of about one hour at a temperature between about 200°C and about 600°C. The encapsulated metal-containing particle may be used to catalyze reactions, including the above-mentioned methods for producing carbon fibrils.

BRIEF DESCRIPTION OF THE FIGURES

Fig. 1. A dispersion of catalyst particles comprised of Fe_3O_4 .

Fig. 2. A dispersion of catalyst particles comprised of Fe_3O_4 .

Fig. 3. Catalyst particles encapsulated in 50-150 angstrom carbon sheaths.

Fig. 4. Numerous 100-450 angstrom diameter fibrils, together with catalyst support and reaction debris.

Fig. 5. A fibril with a diameter of approximately 250 angstroms, together with catalyst support and reaction debris.

Fig. 6. Schematic Diagram of the Continuous Production of Carbon Fibrils.

DETAILED DESCRIPTION OF THE INVENTION

An essentially cylindrical carbon fibril may be produced in accordance with this invention, said fibril being characterized by a substantially constant diameter between 3.5 and about 70 nanometers, a length greater than about 5 times the diameter and less than about 100 times the diameter, an outer region of multiple layers of ordered carbon atoms and a distinct inner core region, each of the layers and the core being disposed concentrically about the cylindrical axis of the fibril. Preferably the entire fibril is substantially free of thermal carbon overcoat. The term "cylindrical" is used herein in the broad geometrical sense, i.e., the surface traced by a straight line moving parallel to a fixed straight line and intersecting a curve. A circle or an ellipse are but two of the many possible curves of the cylinder.

The inner core region of the fibril may be hollow, or may comprise carbon atoms which are less ordered than the ordered carbon atoms of the outer region. "Ordered carbon atoms," as the phrase is used herein means graphitic domains having their c -axes substantially perpendicular to the cylindrical axis of the fibril.

In one embodiment, the length of the fibril is greater than about 20 times the diameter of the fibril. In another embodiment, the fibril diameter is between about 7 and about 25 nanometers. In another embodiment the inner core region has a diameter greater than about 2 nanometers.

A method for producing a carbon fibril according to this invention comprises treating a second essentially

cylindrical discrete carbon fibril characterized by a substantially constant diameter between about 3.5 and about 70 nanometers, length greater than about 10^2 times the diameter, an outer region of multiple essentially continuous layers of ordered carbon atoms and a distinct inner core region, each of the layers and the core being disposed substantially concentrically about the cylindrical axis of the fibril.

It is contemplated that various treating means are suitable for producing the carbon fibril. In one embodiment, treating comprises fragmenting the second carbon fibril by mechanical means, e.g., grinding, milling. In another embodiment, treating comprises altering the second carbon fibril with shear forces that are produced in a fluid medium. More specifically, the second carbon fibril is contained in a liquid or semi-liquid medium, e.g., a monomer or a matrix. The medium is subjected to processing or handling operations, e.g., extrusion, injection, or molding, so as to produce shear forces sufficient to alter the second fibril into a fibril in accordance with this invention.

Another method for producing an essentially cylindrical, discrete carbon fibril according to this invention comprises contacting for an appropriate period of time and at a suitable pressure a catalyst, i.e., a suitable discrete metal-containing particle, with a suitable precursor, i.e., a suitable gaseous, carbon-containing compound, at a temperature between about 850°C and about 1200°C. The ratio on a dry weight basis of carbon-containing compound (precursor) to metal-containing particle (catalyst) is suitably at least about 100:1.

A method for continuously producing carbon fibrils comprises continuously contacting for an appropriate period of time and at a suitable pressure, suitable discrete, metal-containing particles (catalyst), with a suitable gaseous, carbon-containing compound, (precursor), at a temperature between about 850°C and about 1200°C, and recovering the fibrils so produced. In one embodiment, the fibrils may be recovered in association with the metal-containing particles. In another embodiment the fibrils may be separated and recovered from the particles, e.g., by extraction of the metal particles into 10% aqueous solution of hydrochloric acid. The continuous contacting in one embodiment is effected by continuously introducing the precursor into a reaction zone containing the catalyst particles and continuously withdrawing the precursor from the reaction zone, e.g., a flow tower reactor with a packed bed or fluidized bed of catalyst. In another embodiment, contacting is effected by continuously introducing the catalyst particles into a reaction zone containing the precursor and continuously withdrawing the catalyst from the reaction zone. In another embodiment, contacting is effected by continuously introducing both the catalyst particles and the precursor into a reaction zone and continuously withdrawing both from the reaction zone, e.g., a continuous cocurrent or countercurrent flow tower.

In the above-mentioned method for continuously producing carbon fibrils, the withdrawn precursor, catalyst, or both may be treated so as to remove any undesirable material, e.g., impurities, inactive catalyst, or by-products formed during fibril production, and then reintroduced into the reaction zone. In one embodiment where the precursor is carbon monoxide, the effluent

gas, which is predominantly carbon monoxide, carbon dioxide and trace amounts of impurities, may be treated by purging a portion of the effluent gas and adding a relatively pure amount of carbon monoxide. Alternatively, the effluent gas may be treated by scrubbing with a suitable carbon dioxide-absorbing compound such as monoethanolamine (MEA). Still another method of treatment comprises converting the carbon dioxide present in the effluent gas to carbon monoxide, e.g., by passing the effluent gas over or through a carbon source. In an embodiment where the precursor is a gaseous hydrocarbon, treatment of the effluent gas may comprise removing the hydrogen produced during fibril production. In another embodiment where the withdrawn catalyst is treated and reintroduced, treatment may comprise separating the active catalyst from the inactive catalyst by magnetic means.

In another embodiment of the continuous production of carbon fibrils, a portion of the fibrils in association with the metal-containing particles may be continuously recovered, treated with additional metal-containing particles and the fibrils so treated are continuously reintroduced into contact with the gaseous, carbon-containing compound. Treatment may comprise forming a dispersion of catalyst on the fibrils as exemplified in example 38.

It is contemplated that a variety of carbon-containing compounds are suitable as precursors when used with an appropriate combination of reaction parameters, in accordance with this invention. In one presently preferred embodiment, the precursor is carbon monoxide. In other embodiments, suitable precursors include hydrocarbons. A hydrocarbon precursor may be aromatic,

e.g. benzene, toluene, xylene, cumene, ethylbenzene, naphthalene, phenanthrene, anthracene or mixtures thereof. Alternatively, the hydrocarbon may be non-aromatic, e.g. methane, ethane, propane, ethylene, propylene or acetylene or mixtures thereof. In another presently preferred embodiment, the hydrocarbon is methane based upon its availability, thermal stability and lack of toxicity. The hydrocarbon may also contain oxygen, e.g. alcohols such as methanol or ethanol, ketones such as acetone, and aldehydes such as formaldehyde or acetaldehyde or mixtures thereof.

Important reaction parameters, in addition to the particular precursor, include catalyst composition and pretreatment, catalyst support, precursor temperature, catalyst temperature, reaction pressure, residence time or growth time, and feed composition, including the presence and concentrations of any diluents (e.g., Ar) or compounds capable of reaction with carbon to produce gaseous products (e.g., CO₂, H₂, or H₂O). It is contemplated that the reaction parameters are highly interdependent, and that the appropriate combination of the reaction parameters will depend on the specific precursor carbon-containing compound.

It is further contemplated that a variety of transition metal-containing particles are suitable as catalysts when used with an appropriate combination of reaction parameters. In a presently preferred embodiment, the metal-containing particle comprises a particle having a diameter between about 3.5 and about 70 nanometers and contains iron, cobalt or nickel, or an alloy or mixture thereof. Suitable particles may also be derived from metal salts that thermally decompose to metallic particles or metallic oxide particles at temperatures equal

to or below fibril formation temperatures, i.e. below about 1200°C. Such metal salts include carbonates, bicarbonates, nitrates, citrates, and oxalates, e.g., iron oxalate.

In one embodiment, the metal-containing particle is contacted with the carbon-containing compound in the presence of a compound capable of reaction with carbon to produce gaseous products. In one such embodiment, the compound capable of reacting with carbon is CO₂, H₂, or H₂O.

It is desirable that catalyst particles be of reasonably uniform diameter and that they be isolated from one another, or at least held together in only weakly bonded aggregates. The particles need not be in an active form before they enter the reactor, so long as they are readily activated through a suitable pretreatment or under reaction conditions. The choice of a particular series of pretreatment conditions depends on the specific catalyst and carbon-containing compound used, and may also depend on other reaction parameters outlined above. Exemplary pretreatment conditions are provided in the Examples which follow. The metal-containing particles may be precipitated as metal oxides, hydroxides, carbonates, carboxylates, nitrates, etc., for optimum physical form. Well-known colloidal techniques for precipitating and stabilizing uniform, very small particles are applicable. For example, the techniques described by Spiro et al. for precipitating hydrated ferric oxide into easily dispersible uniform spheres a few nanometers in diameter, are very suitable for catalyst preparation, J. Am. Chem. Soc. 88(12):2721-2726(1966); 89(2):5555-5559 and 5559-5562(1967). These catalyst particles may be deposited on chemically com-

patible, refractory supports. Such supports must remain solid under reaction conditions, must not poison the catalyst, and must be easily separated if necessary from the product fibrils after they are formed. Alumina, carbon, quartz, silicates, and aluminum silicates such as mullite may be suitable support materials. For ease of removal, their preferred physical form is thin films or plates which can easily be moved into and out of the reactor. It is further contemplated that carbon fibers or preformed carbon fibrils may be suitable support material.

A preferred method for isolating catalyst particles from one another comprises encapsulating the particles in carbon or a carbon-containing compound, e.g. a carbide, at conditions not conducive to fibril formation. In one embodiment where the catalyst is an iron-containing particle, encapsulation is performed by pretreating the particles for a suitable period to time with a carbon-containing compound, e.g., carbon monoxide or acetylene, at a temperature too low to form fibrils, e.g., below 800°C, so as to encase the particles in carbon or iron carbide. In a preferred embodiment of this method, iron oxalate particles are pretreated for about one hour with a mixture of argon and acetylene in a 9:1 volume ratio at about 400°C. During the pretreatment, the iron oxalate particles are converted by thermal decomposition to iron-containing particles which are encased in a carbon-containing polymer. The encapsulated iron particles may be used in this form as catalyst for fibril formation or the particles may be oxidized under suitable conditions, e.g., contacting with air or a diluted oxygen-containing gas for about 2 hours at 350°C, to form iron oxide particles.

It is further contemplated that the catalyst particles may be encapsulated in an organic polymer, e.g. polystyrene or starch.

It is also contemplated that a higher productivity of carbon fibrils may be achieved by initiating fibril growth throughout the reactor volume. Method of initiating fibril growth include dispersing finely divided and evenly distributed catalyst particles throughout the reactor volume. The particles may be performed or formed by thermolysis of a metal-containing vapor in the reactor itself. For example, iron particles may be formed from ferrocene vapor.

The reaction temperature must be high enough to cause the catalyst particles to be active for fibril formation, yet low enough to avoid significant thermal decomposition of the gaseous carbon-containing compound with formation of pyrolytic carbon. The precise temperature limits will depend on the specific catalyst system and gaseous carbon-containing compound used. For example, benzene is kinetically thermally stable to about 1000°C, methane to about 950°C, and acetylene to about 500°C. In cases where thermal decomposition of the gaseous carbon-containing compound occurs at a temperature near or below that required for an active, fibril-producing catalyst, the catalyst particle may be heated selectively to a temperature greater than that of the gaseous carbon-containing compound. Such selective heating may be achieved, for example, by electromagnetic radiation.

The carbon fibril of this invention may be produced at any desirable pressure, and the optimum pressure will

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be dictated by economic considerations. Preferably, the reaction pressure is between one-tenth and ten atmospheres. More preferably, the reaction pressure is about atmospheric pressure.

In one embodiment, the fibril is produced by contacting for a period of time from about 10 seconds to about 30 minutes and at a pressure of about one atmosphere, a suitable iron-containing particle with gaseous carbon monoxide at a temperature of about 1000°C, the ratio on a dry weight basis of carbon monoxide to iron-containing particle being greater than about 1000:1. In another embodiment the fibril is produced by contacting for from about one minute to about five minutes and at a pressure of about one atmosphere, a suitable iron-containing particle with benzene (gaseous) in an approximately 9:1 hydrogen: benzene mixture at a temperature of about 1100°C, the ratio on a dry weight basis of carbon-containing compound to iron-containing particle being greater than about 1000:1. In a preferred embodiment of this method, the iron-containing particle is supported on a chemically compatible, refractory support, as previously described. Preferably such refractory support is alumina.

Fibrils made according to this invention are highly graphitic as grown. The individual graphitic carbon layers are concentrically arranged around the long axis of the fiber like the growth rings of a tree, or like a scroll of hexagonal chicken wire. There is usually a hollow core a few nanometers in diameter, which may be partially or wholly filled with less organized carbon. Each carbon layer around the core may extend as much as several hundred nanometers. The spacing between adjacent layers may be determined by high resolution elec-

tron microscopy, and should be only slightly greater than the spacing observed in single crystal graphite, i.e., about 0.339 to 0.348 nanometers.

There are no methods for direct measurement of the physical properties of such small fibrils. However, the stiffness of composites containing the fibrils are those expected from the Young's moduli which have been measured on larger, well graphitized carbons.

Another aspect of this invention concerns a method for producing a substantially uniform plurality of essentially cylindrical, discrete carbon fibrils. The plurality of fibrils is substantially uniform in the sense that the diameter of each fibril is substantially equal to the diameter of each other fibril. Preferably each of the fibrils is substantially free of thermally deposited carbon. The method for producing such a plurality involves continuously contacting for an appropriate period of time and at a suitable pressure, suitable metal-containing particles, with a suitable gaseous carbon-containing compound as previously discussed, at a temperature between about 850°C and 1200°C. By this method a substantially uniform plurality of fibrils, e.g. each having a diameter substantially equal to the diameter of each other fibril, may be obtained.

Another aspect of this invention concerns a composite which comprises carbon fibrils as described above, including composites serving as structural materials. Such a composite may also comprise a matrix of pyrolytic or non-pyrolytic carbon or an organic polymer such as a polyamide, polyester, polyether, polyimide, polyphenylene, polysulfone, polyurethane or epoxy res-

in, for example. Preferred embodiments include elastomers, thermoplastics and thermosets.

In another embodiment, the matrix of the composite is an inorganic polymer, e.g. a ceramic material or polymeric inorganic oxide such as glass. Preferred embodiments include plate glass and other molded glass, silicate ceramics, and other refractory ceramics such as aluminum oxide, silicon carbide, silicon nitride and boron nitride.

In still another embodiment the matrix of the composite is a metal. Suitable metals include aluminum, magnesium, lead, copper, tungsten, titanium, niobium, hafnium, vanadium, and alloys and mixtures thereof.

In still another embodiment, the matrix of the composite is an adhesive.

It is contemplated that the carbon fibrils of this invention may be dispersed into the matrix, oriented in the matrix by means of e.g., electrical fields, appropriate shearing action or combing, embedded in the matrix by e.g., impregnation, or injected into the matrix, e.g., by means of spray guns.

Carbon fibrils may also be produced in-situ in porous matrices such as ceramic material. In one embodiment, such in-situ production comprises dispersing catalyst in the ceramic matrix and catalytically growing the fibrils in the matrix by passing a gaseous, carbon-containing compound through the porous ceramic matrix.

It is further contemplated that a plurality of carbon fibrils may be prepared in such a way so as to form a

fibril mat. In one embodiment of the method for continuously producing carbon fibrils, a mat may be produced by collecting or recovering the fibrils on a support plate or filter. Suitable recovery filters include surface filters, e.g. screens, and depth filters, e.g. a bed of sand or body of liquid, including a monomer or low oligomer of a polymer. In another embodiment, the fibrils may be entangled so as to form a mat.

Another aspect of this invention concerns a "furry" fiber, a "furry" plate, or a branched fibril which comprises a carbon fiber, a carbon plate, or a carbon fibril, respectively, and a plurality of carbon fibrils adhering to the outer surface of the fiber, plate, or fibril, respectively. A method for producing furry fibers, furry plates, or branched fibrils comprises dispersing suitable metal-containing particles on the outer surface of a carbon fiber, plate, or fibril, respectively, and contacting with a suitable gaseous, carbon-containing compound for an appropriate period of time and at a suitable pressure.

Another aspect of this invention concerns a composite which comprises fibril mats, furry fibers, furry plates, or branched fibrils, as described above. It is contemplated that fibril mats, furry fibers, furry plates, and branched fibrils may be disposed in a matrix of a composite by the same means described above for carbon fibrils, e.g. dispersion, impregnation, injection, etc.

The carbon fibrils, fibril mats, furry fibers, furry plates and branched fibrils are useful in various applications. One application is a method for reinforcing

ing a structural material by incorporating therein an effective reinforcing amount of carbon fibrils, furry fibers, furry plates, or branched fibrils. Another application is a method for increasing the surface area of an electrode or electrolytic capacitor plate by attaching thereto one or more carbon fibrils, mats, furry fibers, furry plates or branched fibrils. Another application is a method for supporting a catalyst which comprises attaching a catalyst to the fibril, mat, fiber or plate of this invention. Such catalyst may be an electrochemical catalyst.

Still another application is a method of enhancing the electrical conductivity of a material. According to this method an effective electrical conductivity enhancing amount of carbon fibrils, mats, furry fibers, furry plates or branched fibrils is incorporated in the material.

A further use is a method of enhancing the thermal conductivity of a material. In this method an effective thermal conductivity enhancing amount of carbon fibrils, mats, furry fibers, furry plates or branched fibrils is incorporated in the material.

An additional use is a method of shielding an object from electromagnetic radiation by incorporating therein an effective shielding amount of carbon fibrils, mats, furry fibers, furry plates or branched fibrils.

This invention is illustrated in the examples which follow. The examples are set forth to aid in an understanding of the invention but are not intended to, and should not be construed to, limit in any way the invention as set forth in the claims which follow thereafter.

Examples

Materials

The following materials used in the examples below may be obtained from commercial sources: Benzene (reagent grade), $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ (Baker Analyzed Crystal), $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$ (Baker Analyzed Granular), KNO_3 (Baker Analyzed Crystal) and NaHCO_3 (Baker Analyzed Crystal) may all be obtained from J.T. Baker Chemical Company, Phillipsburg, New Jersey. CO (C.P. Grade), hydrogen (H_2), and argon (Ar) may be obtained from Air Products and Chemicals, Inc., Allentown, Pennsylvania. KOH (C.P. Pellets) may be obtained from Mallinckrodt Inc., Lodi, New Jersey. Water used in the examples was deionized. Vycor® glass tubes may be obtained from Corning Glass Works, Corning, New York. Ceramic combustion boats may be obtained from Coors Porcelain Co., Golden Colorado. Iron oxalate crystals (99.999% iron (II) oxalate dehydrate) may be obtained from Aldrich Chemical Company, Inc., Milwaukee, Wisconsin. Starch solution (Corn Products starch 3005) may be obtained from CPC International Inc., Englewood Cliffs, New Jersey. Diglycidyl ether of bisphenol A (DGEBA) (Araldite 6005) may be obtained from Ciba-Geigy Corp., Ardsley, New York.

Davison SMR-37-1534 SRA alumina is an α -boehmite with an average crystallite size of 15 angstroms, an average agglomerate size of 0.2 microns, and an average particle size of 15 microns.

Degussa Aluminum Oxid C is a γ -alumina with a surface area of $100 \text{ m}^2/\text{g}$, an average particle size of 200 angstroms, and an apparent bulk density of 60 g/L.

Cabot Sterling R V-9348 carbon powder is a furnace black with a minimum carbon content of 99.5%, a surface area of 25 m²/g, an average particle size of 750 angstroms, and an apparent density of 16 lb/ft³.

Analyses

All electron micrographs were obtained from a Zeiss EM-10 Electron Microscope.

Catalyst Preparations

Example 1: Preparation of Catalyst 1

A magnetite dispersion was prepared according to the method of Sugimoto and Matijevic, J. Colloid & Interfacial Sci. 74:227 (1980). Electron microscopy reveals the particle size range to be from 175 to 400 angstroms, with 260 angstroms being the approximate average (Figures 1 and 2).

Example 2: Preparation of Catalyst 2

Into a 4 oz wide-mouth glass jar with a magnetic stirring bar was placed 10 g Davison SMR-37-1534 SRA alumina powder. To the stirred powder 0.81 M Fe(NO₃)₃ in H₂O was added dropwise to the point of incipient wetness. 4.1 mL was required.

Example 3: Preparation of Catalyst 3

A portion of the wet powder obtained in Example 2 was heated in the jar with stirring on a hot plate until dry. The temperature was kept below that at which NO_x evolved.

Example 4: Preparation of Catalyst 4

A portion of Davison SMR-37-1534 SRA alumina powder was calcined in an air stream at 900°C for 90 min in a Vycor® tube. In a 4 oz wide-mouth jar with magnetic stirring bar was placed 1.9977 g of the calcined Al₂O₃. While it was being stirred, 0.81 M Fe(NO₃)₃ solution in H₂O was added dropwise to incipient wetness. 0.6 mL was required. The wet powder was dried with stirring on a hot plate.

Example 5: Preparation of Catalyst 5

Into a .4-in cappable serum polymerization tube was weighed 0.44 g Degussa Aluminum Oxid C (fumed Al₂O₃). The tube was capped and argon sparged, after which 1 mL 0.5 M KOH, 1 mL 2.0 M KNO₃, and 6 mL prefiltered deionized water were injected. The mixture was argon sparged 5 min, then 2.0 mL 0.101 M FeSO₄ was injected. The mixture was sparged with argon 1 min. The tube was placed in a 90°C oil bath and the argon sparge continued for 5 min. Sparging was discontinued and quiescent digestion begun. (The oil bath temperature control was faulty, and temperature rose to 105°C. The bath was cooled back to 90°C.) Total digestion time was 2 h.

The system on standing separated into a white precipitate and clear supernate. It was centrifuged, the supernate decanted, the precipitate resuspended in prefiltered, deionized water. This was repeated two more times. The pH on the final supernate was approximately 8.5. The water was decanted, the precipitate blown semi-dry with argon, and resuspended in ethanol.

Example 6: Preparation of Catalyst 6

A portion of Davison SMR-37-1534 SRA alumina powder was calcined 2 h in an air stream at 900°C in a Vycor® tube. One gram of the product was placed in a cappable 4-in polymerization tube and enough 1.6 M $\text{Fe}(\text{NO}_3)_3$ solution was added to cover the alumina completely. The tube was capped and evacuated until bubbling ceased. It was vented and the excess liquid filtered off through an M glass fritted filter. The moist cake was calcined in a ceramic boat for 1 h in an air stream at 500°C.

Example 7: Preparation of Catalyst 7

In a centrifuge bottle 6.06 g $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ was dissolved in 50 mL prefiltered deionized H_2O . To the solution was added 2.52 g NaHCO_3 . When foaming ceased, the solution was sparged 5 min with argon. The product Fe_2O_3 sol was a clear solution.

A portion of Cabot Sterling R V-9348 carbon powder was calcined in a argon stream in a Vycor® boat in a mullite tube at 1100°C for 1 h. It was cooled to room temperature under argon. Into a 4-in polymerization tube enough carbon was placed to make about 0.25 in layer. The tube was evacuated and 2 mL Fe_2O_3 solution was added. When bubbling ceased, the tube was vented and the suspension filtered on a M-glass fritted funnel. The cake was air-dried and heated for 1 h at 500°C under an argon stream in a Vycor® tube.

Example 8: Preparation of Catalyst 8

In a 4-in polymerization tube a 0.4876 g portion of calcined Cabot Sterling R V-9348 carbon powder was evacuated and 2.0 mL 0.81 M $\text{Fe}(\text{NO}_3)_3$ solution was added. When bubbling ceased, the tube was vented and the cake air-dried.

Example 9: Preparation of Catalyst 9

A pellet was made by compressing Cabot Sterling R V-9348 powder in a stainless die (for making KBR discs for infra-red). 0.12 g of the pellet was evacuated in a 4-in polymerization tube and 0.05 mL of a freshly-prepared Fe_2O_3 sol (prepared as in Example 7) was added. The tube was vented and the solid was air-dried.

Example 10: Preparation of Catalyst 10

In a 4-in polymerization tube, 0.23 g of Davison SMR-37-1534 SRA alumina which had been calcined 2 h at 900°C in air was evacuated and 2.0 mL freshly prepared Fe_2O_3 sol (prepared as in Example 7) was added. The tube was vented and the solid filtered out on an M-glass fritted filter. The cake was air-dried.

Fibril Synthesis Runs

Examples 11-33

Examples 11-33 describe fibril synthesis runs. Table 1 summarizes experimental conditions and results. Unless otherwise stated, the fibril precursor was benzene as an approximately 9:1 hydrogen:benzene mixture, and gas flow rates were 300 mL/min for H_2 and Ar; 300 mL/min CO

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and 100 mL/min H₂ for CO/H₂; 300 mL/min Ar or H₂ through benzene at 20°C for Ar/C₆H₆ or H₂/C₆H₆ (approximately 9:1 volume ratio Ar or H₂/C₆H₆). Air and hydrogen were always separated by a brief argon purge of the reactor. Experimental protocols were similar in each run, and are described in detail for Examples 11, 15 and 28.

a) Example 11

Catalyst prepared according to the method of Example 1 was ultrasonically dispersed in water and transferred to a ceramic boat. The boat was placed in the center of a 1" Vycor® tube in an electric furnace at room temperature. The catalyst was brought from room temperature to 500°C over a 15 minute period under a flow of argon. At this temperature, the gas mixture was changed to a hydrogen: benzene (9:1) mixture. This composition was fed into the reactor for 60 minutes.

The hydrocarbon flow was terminated and replaced by argon, and the reactor cooled to room temperature. The boat was removed from the tube and a quantity of carbon was scraped from it. This carbon was ultrasonically dispersed in ethanol and a 10 microliter sample was examined by electron microscopy. The micrographs revealed that most of the iron particles were encapsulated in 50 to 150 angstrom carbon sheaths (Figure 3).

b) Example 15

Catalyst prepared as in Example 2 was dispersed in a ceramic boat. The boat was placed in a 1" Vycor® tube in the same electric furnace as used in Example 11.

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The furnace temperature was raised from room temperature to 500°C and for 60 minutes under air. The reactor was briefly purged with argon. The temperature was then raised from 500°C to 900°C over a 15 minute period under hydrogen and maintained at 900°C for 60 minutes under that hydrogen flow.

Gas flow was then switched to benzene-saturated hydrogen for 180 minutes at 900°C. After cooling to room temperature under argon a sample was prepared according to the procedure of Example 11, and examined by electron microscopy. Electron micrographs revealed numerous 100-450 angstrom diameter fibrils (Figure 4).

c) Example 28

Catalyst prepared as in Example 3 was dispersed in a ceramic boat. The boat was placed in a 1" mullite tube in the same electric furnace as used in Example 11.

The furnace temperature was raised from room temperature to 500°C over 15 minutes and maintained at 500°C for 60 minutes under air. The reactor was briefly purged with argon. The temperature was then raised from 500°C to 900°C over a 20 minute period under hydrogen and maintained at 900°C for 60 minutes under that hydrogen flow. The temperature was then raised still further to 1100°C over a 20 minute period maintaining the same hydrogen flow.

Gas flow was then switched to benzene saturated hydrogen for 5 minutes at 1100°C. After cooling to room temperature under argon a sample was prepared according to the procedure of Example 11, and examined by electron microscopy. Electron micrographs revealed fibrils

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ranging in diameter from 30 to 300 angstroms (Figure 5).

Table 1: Fibril Synthesis Runs

Example No.	Growth Temp. (°C)	Catalyst No.	Growth Time (min)	Pretreatment Conditions	Fibrils	
					Yes	No
11	500	1	60	25-500° in 15 min (Ar)		N
12	750	11	420	23-750° in 40 min (Ar)		N
13	800	3	15	22-500° in 15 min (air) 500° for 60 min (air) 500-900° in 15 min (H ₂) 900° for 60 min (H ₂) 900-800° in 11 min (H ₂)		N
14	900	12	180	26-350° in 20 min (H ₂) 350° for 15 min (H ₂) 350-400° in 10 min (CO/H ₂) 400° for 210 min (CO/H ₂) 400-900° in 26 min (Ar)	Y	
15	900	2	180	500° for 60 min (air) 500-900° in 15 min (H ₂) 900° for 60 min (H ₂)	Y	
16	900	4	180	24-900° in 35 min (Ar) 900° for 60 min (H ₂)	Y	

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Example No.	Growth Temp. (°C)	Catalyst No.	Growth Time (min)	Pretreatment Conditions	Fibrils	
					Yes	No
17	900	3	15	80-500° in 15 min (air) 500° for 60 min (air) 500-900° in 15 min (H ₂) 900 for 60 min (H ₂)		N
18	900	3	60	22-500° in 15 min (air) 500° for 60 min (air) 500-750° in 10 min (H ₂) 750° for 70 min (H ₂) 750-500° in 15 min (H ₂) 500° for 60 min (Ar/C ₆ H ₆) 500° for 90 min (H ₂) 500-900° in 20 min (H ₂)		N
19	900	9	60	90-900° in 30 min (H ₂) 900° for 60 min (H ₂) 900° for 25 min (Ar)		N
20	900	1	60	26-900° in 25 min (Ar)		N
21	900	1	5	220-900° in 20 min (Ar)		N
22	1000	1	5	252-1000° in 30 min (Ar)		N
23	1000	1	120	31-1000° in 85 min (H ₂ /C ₆ H ₆)		N

Example No.	Growth Temp. (°C)	Catalyst No.	Growth Time (min)	Pretreatment Conditions	Fibrils	
					Yes	No
24	1100	5	5	24-500° in 15 min (Ar) 500-900° in 15 min (H ₂) 900° for 60 min (H ₂) 900-1100° in 15 min (H ₂)		N
25	1100	10	1	24-500° in 55 min (air) 500° for 60 min (air) 500-1100° in 30 min (H ₂) 100° for 30 min (H ₂)		N
26	1100	9	1	140-500° in 10 min (Ar) 500° for 60 min (Ar) 500-1100° in 26 min (H ₂) 1100° for 60 min (H ₂)		N
273	1100	5	5	25-500° in 20 min (Ar) 500-900° in 20 min (H ₂) 900° for 60 min (H ₂) 900-1100° in 15 min (H ₂)		N
28	1100	3	5	25-500° in 15 min (air) 500° for 60 min (air) 500-900° in 20 min (H ₂) 900° for 60 min (H ₂) 900-1100° in 20 min (H ₂)	Y	

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Example No.	Growth Temp. (°C)	Catalyst No.	Growth Time (min)	Pretreatment Conditions	Fibrils	
					Yes	No
29	1100	3	1	85-500° in 10 min (air) 500° for 60 min (air) 500-900° in 20 min (H ₂) 900° for 60 min (H ₂) 900-1100° in 10 min (H ₂)	Y	
30	1100	6	5	42-500° in 15 min (Ar) 500-900° in 15 min (H ₂) 900° for 60 min (H ₂) 900-1100° in 15 min (H ₂)	Y	
31	1100	3	5	26-500° in 20 min (air) 500° for 60 min (air) 500-750° in 10 min (H ₂) 750° for 60 min (H ₂) 750-500° in 10 min (H ₂) 500° for 60 min (Ar/C ₆ H ₆) 500° for 90 min (H ₂) 500-1100° in 30 min (Ar)	Y	
32	1150	8	1	98-500° in 20 min (Ar) 500° for 60 min (Ar) 500-750° in 10 min (H ₂) 750° for 30 min (H ₂) 750-1150° in 20 min (Ar) 1150° for 15 min (Ar)		N

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Example No.	Growth Temp. (°C)	Catalyst No.	Growth Time (min)	Pretreatment Conditions	Fibrils	
					Yes	No
33	1150	7	1	30-1150° in 45 min (H ₂) 1150° for 15 min (H ₂)		N

Footnotes to Table 1

1. Catalyst 1 was heated from 270 to 350° in 10 min under H₂, from 350° to 500° in 30 min under CO/H₂, held at 500° for 240 min under CO/H₂, and cooled to room temperature prior to use.
2. Catalyst 1 was supported on a carbon fiber.
3. Feed was approximately 18:1 H₂:C₆H₆.

Example 34: Production of Encapsulated Iron Catalyst

A ceramic combustion boat was coated with 20 mg iron oxalate crystals and treated at 400°C for one hour with a 9:1 volume ratio Ar:C₂H₂. A uniform dispersion of metallic iron particles or iron-containing particles in a carbon-containing polymer was obtained.

Example 35: Production of Iron Oxide Particles

The uniform dispersion of iron-containing particles prepared in example 34 was heated slowly to avoid large temperature rises and particle fusion in flowing air for 2 hours at 350°C. The carbon-containing compound was burnt off and a powder of 30 to 100 angstroms iron oxide was obtained.

Example 36: Production of Iron Particles

The iron oxide particles prepared in example 35 may be reduced with H₂ to produce iron particles in the 30 to 100 angstroms size range.

Example 37: Production of Fibrils using Iron Oxide Catalyst

The iron oxide particles prepared in Example 35 may be heated to 1100°C in flowing argon and treated for 15 minutes at 1100°C with pure CO. The CO flow is then terminated and replaced by Ar to cool the reactor to room temperature. A quantity of carbon may be scraped from the ceramic boat and ultrasonically dispersed in ethanol and examined by electron microscopy. Carbon fibrils in the range of 30 to 100 angstroms are obtained.

Example 38: Dispersion of Catalyst on Fibrils

Carbon fibrils prepared according to Example 37 may be scraped onto a sintered glass filter funnel and wetted with a freshly prepared 2% solution of starch. While still wet, the fibrils are treated with a 0.81 M $\text{Fe}(\text{NO}_3)_3$ solution. Excess liquid is poured off and the fibrils dried in air overnight at room temperature.

Example 39: Production of Branched Fibrils

A small quantity of the fibrils prepared in example 38 may be scraped into a ceramic boat and placed in a 1" alumina tube in an electric furnace. Argon is passed through the tube as the temperature is increased to 1100°C. Carbon monoxide is introduced for 15 minutes. The CO flow is terminated and replaced by argon while cooling the reactor.

A quantity of carbon may be scraped from the ceramic boat and ultrasonically dispersed in ethanol. A sample may be examined by electron microscopy to observe new carbon fibrils with diameters ranging from 50 to 300 angstroms.

Example 40: Continuous Production of Carbon Fibrils with Recycle of Precursor

A stream consisting of recycle and make-up CO may be fed into a flow tower reactor along with catalyst as prepared in example 38. The flow tower is brick lined and approximately 0.30 meters in diameter and 20 meters in overall height (Figure 6).

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The mixed recycle and make-up CO stream enters the tower at the top and flows down through ceramic strip heaters which bring its temperature to 1100°C. The catalyst is fed by a star feeder into the CO stream.

Gas flow through the reaction zone is 0.16 m/sec and the zone is approximately 10 meters long. The reaction may be terminated by the injection of cold (100°C) gas. Product fibrils are collected on a porous ceramic filter and the effluent gas is recompressed to about 1.3 atmospheres. A small purge is taken from the effluent gas to balance unknown impurities formed in the reactor and contained in the feed CO. The stream passes through a KOH Bed (0.5 m in diameter x 2 m long) before the make-up CO is added. The stream then is divided; 9 g/second being diverted through a heat exchanger and the remaining 3 g/second returns to the reaction tower.

After 3 hours, the system is shut down and cooled and the ceramic filter is removed. The carbon fibrils are obtained matted to the filter. The fibrils may be scraped from the filter and used to form a composite.

Example 41: Composite Preparation

An epoxy resin system having 100 parts by weight DGEBA, 36 parts by weight DDS curing agent and 0.5 parts by weight BF₃ MEA accelerator may be used to wet the mat prepared in example 40 and the resulting mass dried overnight at room temperature. Ten one-inch squares are cut from the dried mat and placed in a heated die. A composite is formed by hot-pressing for 3 hours at 100°C. The composite is removed from the disc and aired for 24 hours at 120°C and 4 hours at 175°C.

What is Claimed is:

1. An essentially cylindrical discrete carbon fibril characterized by a substantially constant diameter between about 3.5 and about 70 nanometers, length greater than about 5 times the diameter and less than about 100 times the diameter, an outer region of multiple essentially continuous layers of ordered carbon atoms and a distinct inner core region, each of the layers and the core being disposed substantially concentrically about the cylindrical axis of the fibril.
2. A fibril of claim 1, wherein the core is hollow.
3. A fibril of claim 1, wherein the inner core region comprises carbon atoms which are less ordered than the ordered carbon atoms of the outer region.
4. A fibril of claim 1, wherein the ordered carbon atoms are graphitic.
5. A fibril of claim 1, wherein the length is greater than about 20 times the diameter.
6. A fibril of claim 1, wherein the diameter is between about 7 and 25 nanometers.
7. A fibril of claim 1, wherein the inner core region has a diameter greater than about 2 nanometers.
8. A plurality of essentially discrete carbon fibrils characterized by a substantially constant diameter between about 3.5 and about 70 nanometers, length greater than about 5 times the diameter and less

than about 100 times the diameter, an outer region of multiple essentially continuous layers of ordered carbon atoms and a distinct inner core region, each of the layers and the core being disposed substantially concentrically about the cylindrical axis of the fibrils.

9. A method for producing a carbon fibril of claim 1 which comprises treating an essentially cylindrical discrete carbon fibril characterized by a substantially constant diameter between about 3.5 and about 70 nanometers, length greater than about 10^2 times the diameter, an outer region of multiple essentially continuous layers of ordered carbon atoms and a distinct inner core region, each of the layers and the core being disposed substantially concentrically about the cylindrical axis of the fibril, so as to produce the carbon fibril.
10. A method for producing a carbon fibril of claim 1 which comprises contacting for an appropriate period of time and at a suitable pressure a suitable metal-containing particle with a suitable gaseous, carbon-containing compound, at a temperature between about 850°C and about 1200°C , the ratio on a dry weight basis of carbon-containing compound to metal-containing particle being at least about 100:1.
11. A method for continuously producing carbon fibrils which comprises continuously contacting for an appropriate period of time and at a suitable pressure suitable metal-containing particles with a suitable gaseous, carbon-containing compound, at a temperature between about 850°C and about 1200°C , and recovering the fibrils so produced.

12. A method of claim 11 wherein the continuous contacting is effected by continuously introducing the gaseous carbon-containing compound into a reaction zone containing the metal-containing particle and continuously withdrawing the gaseous carbon-containing compound from the reaction zone.
13. A method of claim 11, wherein the continuous contacting is effected by continuously introducing the metal-containing particles into a reaction zone containing a defined volume of the gaseous, carbon-containing compound and continuously withdrawing the metal-containing particles from the reaction zone.
14. A method of claim 11, wherein the continuous contacting is effected by continuously introducing the metal-containing particles and the gaseous, carbon-containing compound into a reaction zone and continuously withdrawing the metal-containing particles and the gaseous carbon-containing compound from the reaction zone.
15. A method of claim 12, wherein the withdrawn gaseous carbon-containing compound is treated so as to remove any undesirable material and is then continuously reintroduced into the reaction zone.
16. A method of claim 15, wherein the gaseous carbon-containing compound is carbon monoxide and the treatment comprises removing carbon dioxide from the carbon monoxide withdrawn from the reaction zone.

17. A method of claim 13, wherein the withdrawn metal-containing particles are treated so as to remove any undesirable material and recover carbon fibrils and the particles so treated are then continuously reintroduced into the reaction zone.
18. A method of claim 11, wherein the carbon fibrils are recovered in association with the metal-containing particles.
19. A method of claim 18, wherein the carbon fibrils in association with the particles are continuously recovered.
20. A method of claim 19, wherein a portion of the carbon fibrils in association with the particles so recovered are treated with additional metal-containing particles and the fibrils so treated are continuously reintroduced into contact with the gaseous carbon-containing compound.
21. A method according to claim 11, wherein the contacting of the metal-containing particle with the carbon-containing compound is carried out in the presence of a compound capable of reaction with carbon to produce gaseous products.
22. A method according to claim 21, wherein the compound capable of reacting with carbon is CO_2 , H_2 or H_2O .
23. A method according to claim 11, wherein the carbon-containing compound is carbon monoxide.

24. A method according to claim 11, wherein the carbon-containing compound is a hydrocarbon.
25. A method according to claim 24, wherein the hydrocarbon contains oxygen.
26. A method according to claim 25, wherein the oxygen containing hydrocarbon is formaldehyde, acetaldehyde, acetone, methanol, ethanol, or mixture thereof.
27. A method according to claim 24, wherein the hydrocarbon is aromatic.
28. A method according to claim 27, wherein the aromatic hydrocarbon is benzene, toluene, xylene, cumene, ethylbenzene, naphthalene, phenanthrene, anthracene or mixtures thereof.
29. A method according to claim 24, wherein the hydrocarbon is non-aromatic.
30. A method according to claim 29, wherein the hydrocarbon is methane, ethane, propane, ethylene, propylene or acetylene or mixtures thereof.
31. A method according to claim 30 wherein the hydrocarbon is methane.
32. A method according to claim 11 wherein the metal-containing particle comprises an iron-, cobalt-, or nickel-containing particle having a diameter between about 3.5 and about 70 nanometers.

33. A method according to claim 11 wherein the metal-containing particle is supported on a chemically compatible, refractory support.
34. A method according to 33, wherein the support is alumina.
35. A method according to claim 33, wherein the support is carbon.
36. A method according to claim 35, wherein the carbon is a carbon fiber.
37. A method according to claim 35, wherein the carbon is a carbon fibril.
38. A method according to claim 35, wherein the carbon is a carbon plate.
39. A method according to claim 33, wherein the support is a silicate.
40. A method according to claim 39, wherein the silicate is an aluminum silicate.
41. A method of claim 11, wherein the metal-containing particles are derived from metal salts.
42. A method of claim 41, wherein the metal salt is iron oxalate.
43. A method of claim 11, wherein the metal-containing particles are encapsulated in carbon or a carbon-containing compound.

44. A method of claim 42, wherein the metal-containing particles are encapsulated in an organic polymer.
45. A method of claim 44, wherein the organic polymer is polystyrene.
46. A method of claim 44, wherein the organic polymer is a starch.
47. A method according to claim 11, wherein the period of time is from about 10 seconds to about 30 minutes, the pressure is from about one-tenth atmospheres to about ten atmospheres, the metal-containing particle is an iron-containing particle, the gaseous, carbon-containing compound is carbon monoxide and the temperature is from about 900°C to about 1150°C.
48. A method according to claim 47, wherein the period of time is about 10 minutes, the pressure is about one atmosphere, the carbon-containing compound is carbon monoxide and the temperature is about 1000°C.
49. A method according to claim 47, wherein the period of time is from about one to about five minutes, the pressure is about one atmosphere, the carbon-containing compound is carbon monoxide and the temperature is about 1100°C.
50. A method according to claim 47, wherein the iron-containing particle is supported on a chemically compatible, refractory support.

51. A method according to claim 50, wherein the refractory support is alumina, carbon fiber or carbon fibril.
52. A method according to claim 11 wherein the metal-containing particles are independently heated to a temperature between about 850°C and about 1800°C, the temperature of the particles being higher than the temperature of the gaseous, carbon-containing compound.
53. A method according to claim 52, wherein the particles are heated with electromagnetic radiation.
54. A carbon fibril produced according to the method of claim 10.
55. A method for producing a substantially uniform plurality of essentially cylindrical, discrete carbon fibrils which comprises continuously contacting for an appropriate period of time at a suitable pressure, suitable metal-containing particles with a suitable gaseous carbon-containing compound, at a temperature between about 850°C and 1200°C.
56. A substantially uniform plurality of carbon fibrils produced according to the method of claim 55.
57. A composite which comprises a plurality of carbon fibrils according to claim 1 in a matrix.
58. A composite according to claim 57, wherein the matrix comprises an organic polymer.

59. A composite according to claim 57, wherein the matrix comprises an inorganic polymer.
60. A composite according to claim 57, wherein the matrix comprises a metal.
61. A composite which comprises carbon fibrils dispersed in a matrix.
62. A composite of claim 61, wherein the matrix is an adhesive.
63. A composite of claim 61, wherein the matrix is a ceramic material.
64. A composite of claim 61, wherein the dispersed fibrils are oriented within the matrix.
65. A composite which comprises carbon fibrils of claim 1 and a matrix.
66. A composition of matter which comprises a metal-containing particle supported on a fibril.
67. A fibril mat comprising a plurality of fibrils.
68. A composite which comprises the fibril mat of claim 67 and a matrix.
69. A furry fiber comprising a carbon fiber and a plurality of carbon fibrils adhering to the outer surface of the fiber.

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70. A furry plate comprising a carbon plate and a plurality of carbon fibrils adhering to the outer surface of the plate.
71. A composition of matter which comprises a first carbon fibril and a plurality of fibrils adhering to the outer surface of the first fibril.
72. A method of preparing a composite of claim 61 which comprises producing the carbon fibrils as a dispersion in the matrix.
73. A method of preparing a composition of matter claim 66 which comprises dispersing metal-containing particles on the outer surface of the fibril.
74. A method of producing a fibril mat of claim 67 which comprises preparing a plurality of carbon fibrils so as to form a fibril mat.
75. A method of preparing a composite of claim 68 which comprises impregnating a fibril mat with a matrix.
76. A method of preparing the furry fiber of claim 69 which comprises dispersing a plurality of metal-containing particles on the outer surface of a carbon fiber and contacting for an appropriate period of time and at a suitable pressure, the carbon fiber with a suitable gaseous, carbon-containing compound so as to produce carbon fibrils which adhere to the outer surface of the fiber.
77. A method of preparing the furry plate of claim 70 which comprises dispersing a plurality of metal-

containing particles on the outer surface of a carbon plate and contacting for an appropriate period of time and at a suitable pressure, the plate with a suitable gaseous, carbon-containing compound so as to produce carbon fibrils which adhere to the outer surface of the plate.

78. A method of preparing a composite of claim 65 which comprises dispersing fibrils of claim 1 in a matrix.
79. A method of reinforcing a structural material which comprises incorporating therein an effective reinforcing amount of carbon fibrils according to claim 1.
80. A method of enhancing the electrical conductivity of a material which comprises incorporating therein an effective electrical conductivity-enhancing amount of carbon fibrils according to claim 1.
81. A method of enhancing the thermal conductivity of a material which comprises incorporating therein an effective thermal conductivity-enhancing amount of carbon fibrils according to claim 1.
82. A method of increasing the surface area of an electrode or an electrolytic capacitor plate which comprises attaching thereto one or more fibrils according to claim 1.
83. A method of supporting a catalyst which comprises attaching a catalyst to a fibril according to claim 1.

84. A method according to claim 83, wherein the catalyst is an electrochemical catalyst.
85. A method of shielding an object from electromagnetic radiation which comprises incorporating therein an effective shielding amount of carbon fibrils according to claim 1.
86. A method of reinforcing a structural material which comprises incorporating therein an effective reinforcing amount of fibril mats according to claim 67.
87. A method of enhancing the electrical conductivity of a material which comprises incorporating therein an effective electrical conductivity-enhancing amount of fibril mats according to claim 67.
88. A method of enhancing the thermal conductivity of a material which comprises incorporating therein an effective thermal conductivity-enhancing amount of fibril mats according to claim 67.
89. A method of increasing the surface area of an electrode or an electrolytic capacitor plate which comprises attaching thereto one or more fibril mats according to claim 67.
90. A method of supporting a catalyst which comprises attaching a catalyst to a fibril mat according to claim 67.
91. A method according to claim 90, wherein the catalyst is an electrochemical catalyst.

92. A method of shielding an object from electromagnetic radiation which comprises incorporating therein an effective shielding amount of fibril mats according to claim 67.
93. A method of reinforcing a structural material which comprises incorporating therein an effective reinforcing amount of furry fibers according to claim 69.
94. A method of enhancing the electrical conductivity of a material which comprises incorporating therein an effective electrical conductivity-enhancing amount of furry fibers according to claim 69.
95. A method of enhancing the thermal conductivity of a material which comprises incorporating therein an effective thermal conductivity-enhancing amount of furry fibers according to claim 69.
96. A method of increasing the surface area of an electrode or an electrolytic capacitor plate which comprises attaching thereto one or more furry fibers according to claim 69.
97. A method of supporting a catalyst which comprises attaching a catalyst to a furry fiber according to claim 69.
98. A method according to claim 97, wherein the catalyst is an electrochemical catalyst.
99. A method of shielding an object from electromagnetic radiation which comprises incorporating therein an effective shielding amount of furry fibers according to claim 69.

100. A method of reinforcing a structural material which comprises incorporating therein an effective reinforcing amount of furry plates according to claim 70.
101. A method of enhancing the electrical conductivity of a material which comprises incorporating therein an effective electrical conductivity-enhancing amount of furry plates according to claim 70.
102. A method of enhancing the thermal conductivity of a material which comprises incorporating therein an effective thermal conductivity-enhancing amount of furry plates according to claim 70.
103. A method of increasing the surface area of an electrode or an electrolytic capacitor plate which comprises attaching thereto one or more furry plates according to claim 70.
104. A method of supporting a catalyst which comprises attaching a catalyst to a furry plate according to claim 70.
105. A method according to claim 104, wherein the catalyst is an electrochemical catalyst.
106. A method of shielding an object from electromagnetic radiation which comprises incorporating therein an effective shielding amount of furry plates according to claim 70.
107. A composition of matter comprising a plurality of discrete, unfused, metal-containing catalytic

particles encapsulated in carbon or a carbon-containing compound, the particles so encapsulated remaining unfused at temperatures greater than about 350°C.

108. A composition of matter of claim 107, wherein the particles are iron-, cobalt-, or nickel-containing particles having diameters between about 3.5 and 70 nanometers.
109. A composition of matter of claim 108, wherein the particles are iron-containing particles.
110. A composition of matter of claim 108, wherein the particles are derived from a metal salt that thermally decomposes to metal or metal oxide particles.
111. A composition of matter of claim 110, wherein the metal salt is iron oxalate.
112. A composition of matter of claim 107, wherein the particles are supported on a chemically compatible, refractory support.
113. A composition of matter of claim 112, wherein the support is carbon, carbon fiber or a carbon fibril.
114. A composition of matter of claim 107, wherein the particles are encapsulated in an organic polymer.
115. A composition of matter of claim 114, wherein the organic polymer is polystyrene.

116. A composition of matter claim 114, wherein the organic polymer is a starch.
117. A method of catalyzing a reaction which comprises incorporating into the reaction the catalyst of claim 107.
118. A method of preparing the catalytic particles of claim 107 which comprises treating for an appropriate period of time and at a suitable temperature below 800°C, metal-containing particles with a carbon-containing compound so as to encapsulate the particles in a carbon-containing compound.
119. A method of claim 118, wherein the metal-containing particle is an iron-containing particle.
120. A method of claim 118, wherein the carbon-containing compound is CO.
121. A method of claim 118, wherein the carbon-containing compound is acetylene.
122. A method of claim 118, wherein the period of time is about one hour, the temperature is from about 200°C to about 600°C, the metal-containing particle is iron oxalate, and the carbon-containing compound is acetylene.
123. A method for producing an essentially cylindrical, carbon fibril which comprises contacting for an appropriate period of time and at a suitable pressure, an iron-containing particle of claim 111 with a suitable gaseous, carbon-containing compound, at a temperature between about 850°C and about 1200°C.

FIG. 1



Fe_3O_4

38000x

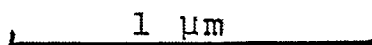


FIG. 2



Fe_3O_4 1 μm 47000x

FIG. 3

0.5 μm 47100x



FIG. 4

1 μm

6200x

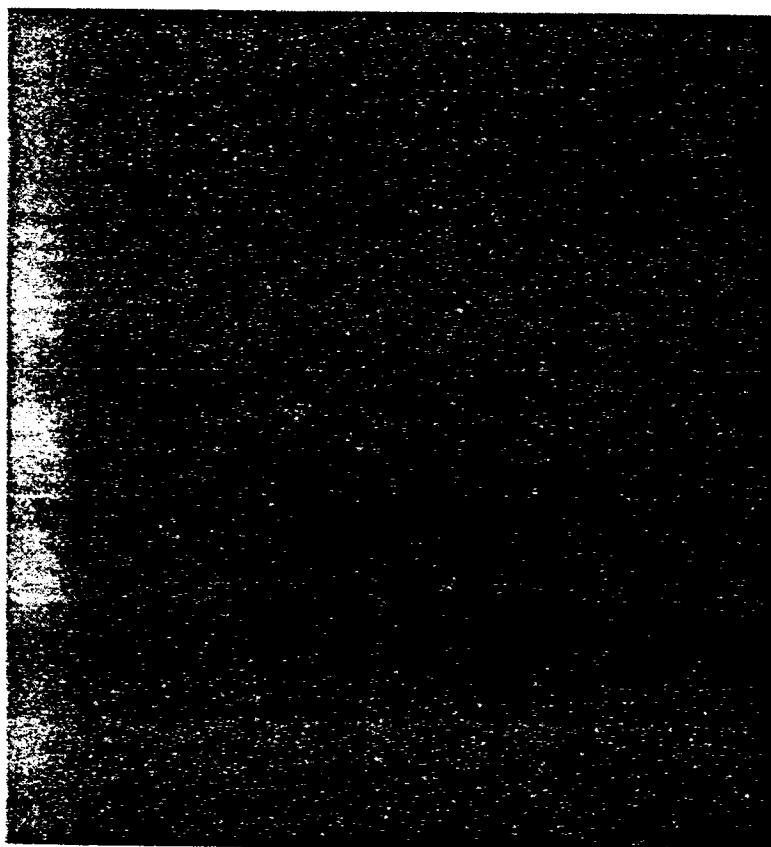


FIG. 5

0.5 μm 37800x

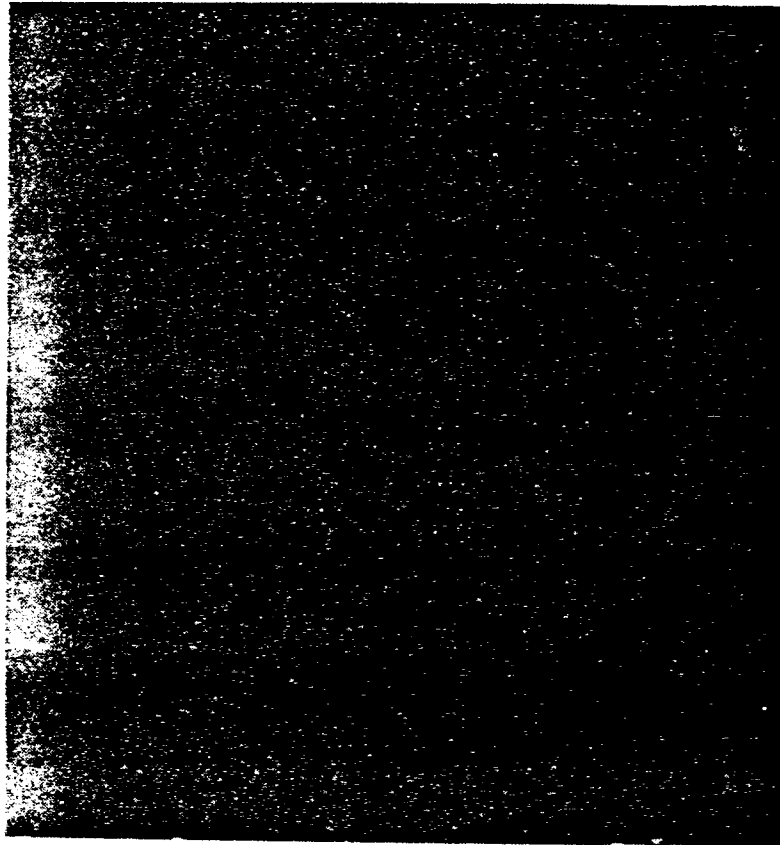
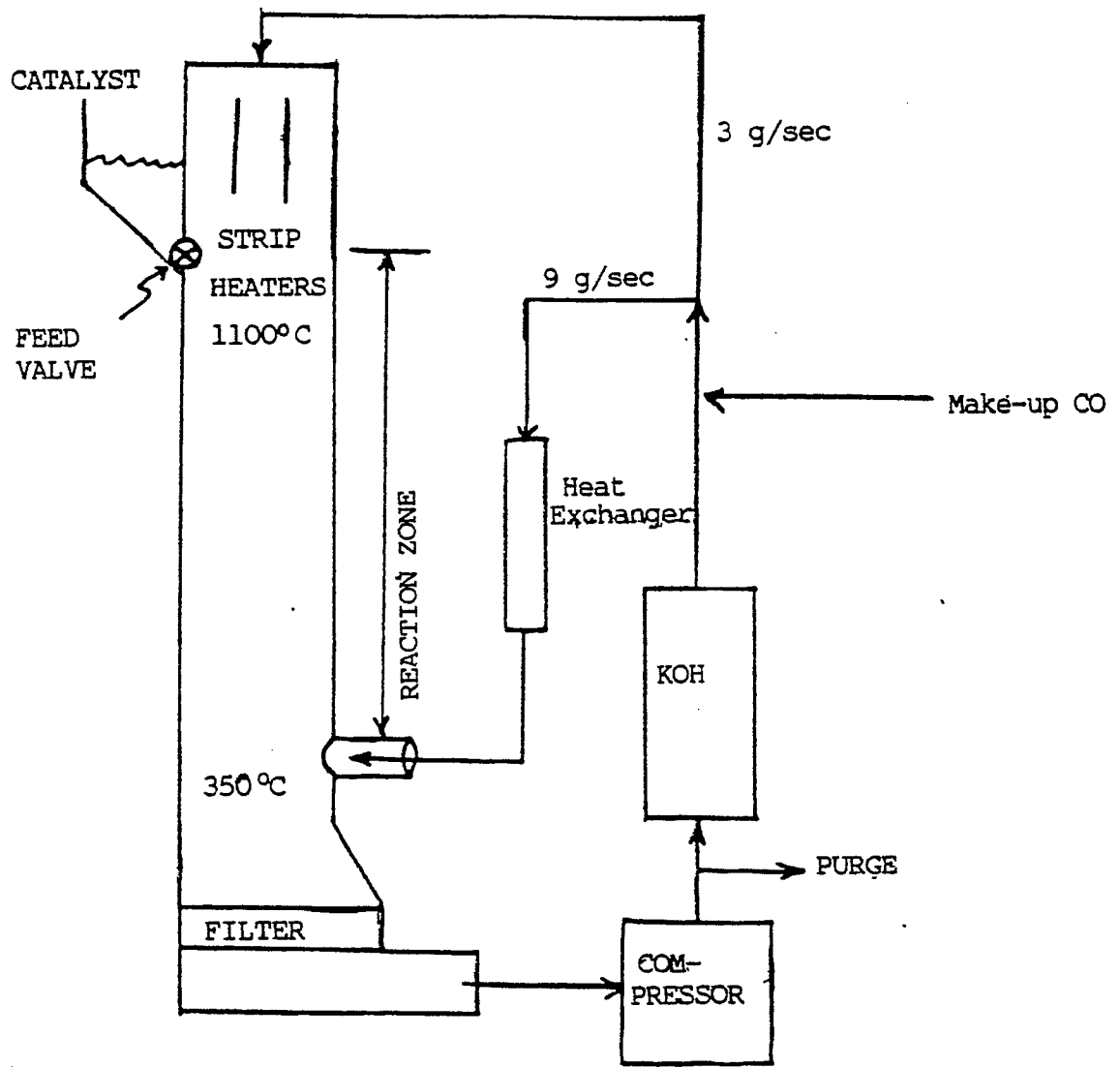



FIG. 6



INTERNATIONAL SEARCH REPORT

International Application No **PCT/US87/01317**

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) ³		
According to International Patent Classification (IPC) or to both National Classification and IPC		
INT. CL.4 B32B 9/00		
US CL. 427/216, 249, 255.1; 428/284, 367, 376, 398, 403, 408		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁴		
Classification System	Classification Symbols	
U.S.	427/216, 249, 255.1 428/284, 367, 376, 398, 403, 408	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁵		
III. DOCUMENTS CONSIDERED TO BE RELEVANT ¹⁴		
Category *	Citation of Document, ¹⁵ with indication, where appropriate, of the relevant passages ¹⁷	Relevant to Claim No. ¹⁸
X, P	US, A, 4,663,230 (TENNET) 05 MAY 1987 See entire document.	1-123
<p>* Special categories of cited documents: ¹⁵</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&" document member of the same patent family</p>		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search ²	Date of Mailing of this International Search Report ³	
20 OCTOBER 1987	03 NOV 1987	
International Searching Authority ¹	Signature of Authorized Officer ²⁰	
ISA/US	 W.J. VanBalén	