# **ClO2**를 이용한 **SO2**와 **NOx** 제거 반응 메커니즘

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#### **Reaction mechanism in the Sulfur dioxide and Nitric oxide Removal using Euchlorine Gas**

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## **1. Introduction**

Combustion of fossil fuel results in emission of  $SO_2$  and  $NO_x$ . Among various technologies conventionally used for removal of  $SO<sub>2</sub>$  and NO, scrubbing methods are economically most competitive and have advantage of controlling other acid gases and particulates at the same time [Yang et al., 1996]. No efforts ever have been made to utilize  $ClO<sub>2</sub>$  gas in the removal of SO<sub>2</sub> and NO from the flue gas. This has promoted us to clean up  $NO<sub>x</sub>$  and  $SO<sub>2</sub>$  simultaneously from flue gas by passing chlorine dioxide gas into the scrubbing solution.

 Chlorine dioxide is powerful oxidant and disinfectant. In the recent years, it has attracted significant commercial attention not only due to environmental concern but also due to its wide applications in the fields of bleaching, oxidation and disinfection. Chlorine-dioxide can be formed by reduction of chlorate with a wide variety of reducing agents in a relatively concentrated acid solution as follows:

 $ClO_3 + 2H^+ + e^- \rightarrow ClO_2 + H_2O$  (1)

The choice of reducing agent has a great bearing on the optimum reaction conditions, by-products and the economics of the process. In all chlorate based processes, chloride ion plays a crucial role. No chlorine dioxide is formed if chloride ion is not present in the reaction medium. With this view, we selected chlorate-chloride process to generate  $ClO<sub>2</sub>$  gas for further use in removing  $SO<sub>2</sub>$  and NO from the flue gas. The general stoichiometry of chloride-chlorate process [Deshwal and Lee, 2004, Hong et al., 1967] can be expressed as:

$$
4H^{+} + 2ClO_{3}^{-} + 2Cl \rightarrow 2ClO_{2} + Cl_{2} + 2H_{2}O
$$
\n(2)

This process is extremely simple to operate, responds immediately and gives highest yield of  $ClO<sub>2</sub>$  at the lowest cost among all other commercial processes.

#### **2. Experimental Section**

 The experimental system as shown in Figure 1 is divided into two parts i.e. chlorine dioxide generation unit and flue gas treatment unit. Chlorine dioxide generation unit is composed of a reactor which is a well stirred sealed vessel having total volume of 2.5L. Concentrated sodium chloride solution (2M) was continuously injected into reactor at a suitable flow rate by syringe pump. The reactor was filled with 1.5L solution of sodium chlorate (0.4M) in a relatively concentrated sulfuric acid  $(\sim 12N)$ . Continuous stirring was provided by a mechanical agitator. Temperature of the reaction vessel was controlled within  $45 \pm 0.1^{\circ}$ C by water thermostat. The reactor was wrapped with an aluminium foil to avoid any photo-dissociation of chlorine dioxide. Nitrogen gas was purged through the reaction mixture using a bubbling device at a flow rate of  $2L/min$ . Chlorine-dioxide carried by N<sub>2</sub> gas was further introduced into bubbling reactor.

Flue gas cleansing unit composed of simulated flue gas supply system, bubbling reactor, pH control system, ClO<sub>2</sub> absorber, data acquisition system, and sampling cum analysis system. The simulated flue gas was obtained by controlled mixing of  $SO_2$ ,  $NO$ ,  $N_2$  and  $O_2$  using mass flow controllers. Continuous stirring was provided by mechanical agitator with a speed of 250rpm. Temperature of the reaction vessel was controlled within  $45 \pm 0.1^{\circ}$ C. The pH of reaction solution was controlled by using an auto-pH control system by continuous addition of NaOH (0.2M) solution with the help of peristalsis pump. The chlorine dioxide absorber (2L vessel) consisted of ca. 2% carbonate buffered potassium iodide solution (1.5L). Samples from reactor and absorber were analyzed using either ion chromatograph (IC) or iodometrically with the help of auto-titrator (Metrohm-Swiss). The  $SO<sub>2</sub>$  and NOx concentrations of inflow gas were analyzed using the gas analyzers (Ultramat 23, Siemens, Germany and Model: 42C, Thermo Environmental Instruments Inc., USA) after removing the moisture in the sample conditioner.

## **3. Results and discussion**

There is no doubt about the oxidizing capability of  $ClO<sub>2</sub>$ . It can oxidize NO into NO<sub>2</sub>; therefore it may prove useful for removal of NO from the flue gas. With this view, experiments for removal of NO and simultaneous removal of  $SO<sub>2</sub>$  and NO have been conducted using chlorine dioxide. A plausible mechanism has also been proposed.

## **3.1. Removal of Nitric oxide**

 Experiments were carried out at pH of 3.5 and input NO concentration of 500ppm in absence of input  $SO_2$  at 45°C to investigate the  $\overline{NO_x}$  removal using chlorine-dioxide. NO<sub>x</sub> removal efficiency and ion concentration measured by ion chromatograph are plotted versus time in Figure 2. It was observed that  $ClO<sub>2</sub>$  can oxidize NO into NO<sub>2</sub> completely and a consistent and reproducible NO<sub>2</sub> absorption efficiency of about 60% is maintained.

# **3.2. Simultaneous removal of sulfur dioxide and nitric oxide**

Simultaneous removal of  $SO_2$  and NO was also studied at input  $SO_2$  and NO concentration of 500 and 350ppm respectively at pH of 3.5 at 45 $^{\circ}$ C. SO<sub>2</sub> and NO<sub>x</sub> removal efficiencies are presented in Figure 3. It is observed that  $ClO<sub>2</sub>$  can clean up both  $SO<sub>2</sub>$  and NO quite efficiently. The maximum DeSO<sub>y</sub> and DeNO<sub>y</sub> efficiency obtained at an optimum NaCl (2M) feeding rate of 0.5ml/min are about 100 and 60% respectively.

# **3.3. Mechanism Involved in the removal of SO<sub>2</sub> and NO using chlorine-dioxide**

# *In the acidic medium*:

NO and  $SO<sub>2</sub>$  removal by chlorine-dioxide is considered to follow the following mechanism:



The overall reaction for  $NO<sub>x</sub>$  removal can be written as:

 $5NO + 3ClO<sub>2</sub> + 4H<sub>2</sub>O \rightarrow 5HNO<sub>3</sub> + 3HCl$  (6) Chlorine gas produced along with chlorine dioxide as suggested in Eq. (2) is also a strong oxidant. Yang et al.  $[1996]$  reported that chlorine is capable of oxidizing NO into NO<sub>2</sub> and nitrate. Stoichiometry of reaction of chlorine with NO can be expressed as:

 $NO + Cl<sub>2</sub> + H<sub>2</sub>O \rightarrow NO<sub>2</sub> + 2HCl$  (7)

 $2NO + 3Cl<sub>2</sub> + 4H<sub>2</sub>O \rightarrow 2HNO<sub>3</sub> + 6HCl$  (8) Formation of sulfate, nitrate and chloride as suggested above is confirmed by analyzing the sample

from bubbling reactor using ion chromatograph and variation of ion concentration with time is presented in Figure 2 and 4.

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# **3.4. Effect of pH:**

The pH of reaction medium is a crucial parameter in the removal of  $SO<sub>2</sub>$  and NO. In the present study, pH of reaction medium was varied from 3.5 to 11 at constant input NO concentration of 500ppm in absence of  $SO_2$  at 45°C and its effect on  $NO_x$  removal is reported in Figure 5. At constant NaCl(2M) feeding rate of 0.5ml/min, there occurred no change in the  $NO<sub>x</sub>$  removal efficiency when pH is increased from 3 to 6 but thereafter removal efficiency decreased until pH 8 and again increased up to pH 9 and attained a steady state. It may be attributed due to different mechanism involved in NOx removal at different pH. When pH reaches neutrality, the disproportionation [White et al., 1942] of chlorine dioxide starts and it leads to formation of chlorite and chlorate as follows:

 $2ClO<sub>2</sub> + 2NaOH \rightarrow NaClO<sub>2</sub> + NaClO<sub>3</sub> + H<sub>2</sub>O$  (9)

So 50% of ClO<sub>2</sub> is converted into chlorite which is again a strong oxidant and absorbent for NO and NO2 respectively. NOx removal mechanism changes when medium of solution changes from acidic (pH < 7) to alkaline (pH > 7). The decrease in  $NO_x$  removal efficiency at pH around 7 or above is believed due to insufficient chlorite in reaction solution. The  $NO<sub>x</sub>$  removal mechanism in alkaline medium can be summarized as:

## *In Alkaline Medium:-*

 $2NO + NaClO<sub>2</sub> \rightarrow 2NO<sub>2</sub> + NaCl (oxidation)$  (10)

 $4NO<sub>2</sub> + NaClO<sub>2</sub> + 4NaOH \rightarrow 4NaNO<sub>3</sub> + NaCl + 2H<sub>2</sub>O (absorption)$  (11) The overall reaction can be written as:

 $4NO + 3NaClO<sub>2</sub> + 4NaOH \rightarrow 4NaNO<sub>3</sub> + 3NaCl + 2H<sub>2</sub>O$  (12)

The above mechanism has been discussed in detail by several workers [Sada et al., 1979, Brogen et al., 1998] To confirm the belief that  $NO<sub>x</sub>$  removal mechanism changes in the alkaline medium, the NaCl feeding rate was enhanced so that more chlorite is formed by disproportionation of unused dissolved  $ClO<sub>2</sub>$  and it was found that  $NO<sub>x</sub>$  removal attained a steady state at higher NaCl feeding rate due to formation of sufficient chlorite. At NaCl(2M) feeding rate of 1.5ml/min, constant  $NO<sub>x</sub>$  removal efficiency of around 60% was achieved in the wide pH range of 3 to 11.

# **4. Conclusions**

## *Merits of using ClO<sub>2</sub> in SO<sub>2</sub> and NO<sub>x</sub> removal*

Chlorine dioxide has proved most promising chemical for simultaneous removal of  $SO<sub>2</sub>$  and NO. The merits of chlorine dioxide can be summarized as:

- 100% SO<sub>2</sub> removal efficiency, 100% NO oxidation and  $\sim 60\%$  NO<sub>x</sub> removal efficiency.
- Low capital cost,
- pH needs no tight control. It is as effective at low pH as at high pH.
- Operation of the system is comparatively easier.
- Easy to handle the waste water

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Fig. 1. A schematic diagram of the experimental apparatus. Fig.2.  $NO<sub>x</sub>$  removal and ion concentration with passage of time using chlorine dioxide.



Fig. 3. Simultaneous removal  $SO_2$  and  $NO_x$  with time using chlorine dioxide.



Fig. 4. Variation in ion concentration with time on passing chlorine dioxide in simultaneous removal  $SO<sub>2</sub>$  and  $NO<sub>x</sub>$ .



Fig. 5. Effect of pH on  $NO<sub>x</sub>$  removal at constant NO input concentration of 500ppm at 45°C

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