P287 **Chap. 10 Optical properties**

P296 (EX 10.1) Estimate the refractive index of PF

P303 (Ex10.2) Estimate the opticalstress coeff. For polycarbonate with Vw=144 cm3 /mol

P311 (Ex 10.3) Estimate the specific refractive index increment (dn/dc) of polystylene in 1, 4 – dioxane $(n_d=1.422)$

Chap. 11 Electrical poroperties

P324 (Ex11.1) Estimate the dielectric constant and the average dipole moment of polycarbonate

P325 correlation between dielectric constant and solubility parameter (see Table 11.4)

 $\delta = 7.0 \,\mathrm{G}$ (11.5)

p330 conductivity (see Fig 11.5)- p.332

p343 **Chap. 12 Magnetic properties**.

Chap. 13 Mechanical Properties of Solid Polymer

p.367 • Hook's Law

 $\tau = Y \epsilon$, stress is proportional to the strain

τ : stress Є : strain Y : young's modulus

(a) Tensile deformation

- tensile strain :
- tensile stress : $\sigma = f/A$
- tensile modulus : $Y = \tau / \mathcal{E}$
- tensile compliance : $D = \theta / \tau$

λ λ $-$ λ 0 $-\lambda$

(b) shear deformation

- shear strain: $\gamma = \tan \alpha = \frac{dy}{dx}$ *dy*
- shear stress: $\sigma = f/A$
- shear modulus : $G = \sigma / \gamma$
- shear compliance : $J = \gamma / \sigma$

(see Table 13.1)

• A modulus is the ratio between the applied stress and the corresponding deformation.

a fuid surface at y:

velocity :
$$
y = \frac{dX}{dt}
$$

• a fluid surface at y+dy : velocity : y+dy:

• shear strain :
$$
\gamma = \frac{dX}{dy}
$$

• shear rate : $\acute{r} = \frac{d}{dt}(y) = \frac{d}{dt} \left(\frac{dx}{dy} \right) = \frac{d}{dy} \left(\frac{dx}{dt} \right) = \frac{dx}{dt}$ *dt dx dy d dy dx dt d* $\frac{d}{dt}(\gamma) = \frac{d}{dt} \left(\frac{dx}{dy} \right) = \frac{d}{dy} \left(\frac{dx}{dt} \right) =$ J $\left(\frac{dx}{1}\right)$ $=\frac{d}{dy}\left($ J \backslash $\overline{}$ J $(\gamma) = \frac{d}{\gamma}$

an alternate definition of the shear rate is the velocity gradient du/dy

• shear stress :
$$
\tau = \frac{F(in \ x \ direction)}{A(in \ y \ direction)} \frac{(force)}{(length^2)}
$$

• viscosity:
$$
\eta = \tau / f
$$

p369• Poisson Ration :
$$
v = \frac{change}{change}
$$
 in width per unit width
change in length per unit length

 $=$ $=$ *axial strain lateral contraction*

• poisson ratio 비교, Table 13.4 (p.374)로부터 PMMA, $v = 0.40$ PS 0.38 Copper 0.34 Glass 0.23

p. 377

 (Ex.13.1) Estimate the bulk modulus of a medium density polyethylene, density of 0.95 (degree of crystallinity = 70%)

(sol.) (a) Estimation by Rao fuction: 식 (13.22)로부터 (p. 375) $K/_{\rho} = \begin{pmatrix} U_R \ W \end{pmatrix}$ ſ *V* $\left(U_{R}\diagup\right)^{6}$ molar volume, $V = \frac{M}{\rho}$ $\frac{M}{\rho}$ = $\frac{28}{0.95}$ = 29.5 (cm³/mol)

여기서 U (Molar elastic Wave Fuction)를 구하기 위하여 Table 14.2 참조 (p.447) $U_R = 2 \times 880 \text{ (cm}^3/\text{mol}) \text{ (cm/sec)}^{1/3}$ $= 1760$

$$
\exists \exists \exists \exists \in \left(\frac{U_R}{V} \right)^6 = \left(\frac{1760}{29.5} \right)^6
$$

= 4.5 x 10¹⁰(cm²/sec²)

$$
\therefore \text{ K} = 4.5 \text{ x } 10^{10} \text{ x } 0.95 \text{ g/cm} \cdot \text{ sec}^2
$$

=
$$
\frac{4.3 \text{ x } 10^9 \text{ (N/m}^2)}{49.5 \text{ N/m}^2}
$$

p378 (Ex 13.2) Estimate the moduli and Poisson ratio of polycarbonate, (sol.) Poisson ratio ;

$$
\begin{array}{rcl} \n\text{A} & (13.10) & \text{(p. 370)} \, \text{O} \, \text{E} \, \text{H} \, \text{E} \\
\text{v} & = & \frac{1 - \frac{2G}{3K}}{2(1 + \frac{G}{3K})} = \frac{1 - 0.15}{2(1 + 0.075)} = 0.39\n\end{array}
$$

$$
v \quad (exp) = \underline{0.39}
$$

p388. • Linear Viscosity.

 ¡) Linear elastic model : OR Hookean Solid. $\tau = G \gamma$

G= shear modulus

Linear elastic model

τ : G^γ

G: shear modulus

Or Hookean solid • The overall modulus is a function of time only, no the magnitude of Stress or strain.

$$
G\equiv\frac{\tau}{\gamma}=G
$$

(t only for linear response)

Fig. Response of dashpot


```
Or Newtonian fluid
```

$$
\tau=\eta\,f
$$

η:viscosity

• **Mechanical Models for linear viscoelasic response**

(1) The Maxwell Element.

- a simple series combination of a linear viscous element (dashpot) and a linear elastic element (spring)

 -the spring and dashpot support the same stress: $\tau = \tau_{\text{spring}} = \tau_{\text{dashpot}}$

-the overall strain of the element :

 $\gamma = \gamma$ spring + γ dashpot
differentiation with $\begin{bmatrix} F_i \end{bmatrix}$ Maxwell differentitation with time, t $\dot{\mathbf{r}} = \dot{\mathbf{r}}_{\text{spring}} + \dot{\mathbf{r}}_{\text{dashpot}}$ $\acute{\textbf{r}} = \acute{\textbf{r}}/\textbf{G} + \tau / \textbf{n}$ **Fig. Maxwell element** $\tau = \eta_i f - (\eta_i / G) \tau_i$ $=$ $n \dot{r} - \lambda \dot{\tau}$ where $(\lambda = \eta/G$: relaxation time)

• creep test – a constant stress is instantaneously applied to the material, and the resulting strain is followed as a function of time

• creep recovery : deformation after removal of the stress.

 τ_0/G : instantaneous stretching of the spring to an equilibrium value with the sudden application of stress (τ_0)

Elastic Recovery: when the stress is release the spring immediately contracts by an amount equal to its original extension

Stress relaxation test : Suddenly applying a strain to the sample and following the stress as a function of time as the strain is held constant.

 λ : (relaxation time)- time required for the stress to decay to a factor of 1/e or 37% of its initial value.

- 실제 linear polymer 의 stress-relaxation curve 와 비슷함

(ⅱ**) The Voigt-kelvin Element : for crosslinked polymer**

- strain in each element is same
- $\gamma = \gamma$ spring = γ dashpot
- The stress is the sum of the stresses:

 $\tau = \tau_{spring} = \tau_{dashpot}$ $\tau = G \gamma + \eta \dot{\tau}$

• **Creep response of a Voigt-kelvin Element : stress is constant**

-initial slope of the strain vs time curve is

- as the element is extend, the spring provides an increasingly greater resistance

to further extension, and so the rate of creep decreases.

- Eventually, the system curves to equilibrium with the spring alone supporting the stress. (rate of strain = 0 , resistance of the dashpot= 0)
- The equilibrium strain = τ_0/G
- Voigt-kelvin model : a fair qualitative picture of the creep respose of some crosslinked polymers.
- characteristics of tensile stress-strain curves of polymer samples.

See page 413 in V. K.

- polymer 사이에 dipole-dipole interaction 이 없기 때문에 soft 하다.
- strongly polar polymer: Nylon, PC, acetal (Engineering plastics) see P.426

- yield stress : 11000psi
- strain at yield : 15%
- ultimate elongation : 80%
- Filled thermosetting polymers:

일반 engineering 고분자와 비교했을 때 stiffness 가 4-5 배

• high modulus, high strength polymer – Aramid Fiber (Kevlar) – aromatic polyamid. Thermosetting resin, carbon Fiber 등의 액정고분자

p402 C5. The time-temperature superposition principle (TTSP)

- Above Tg, the stress relaxation and the creep behavior of amorphous polymers obey the " time-temperature superposition principle"
- In viscoelastic maters, time and temperature are equivalent to the extent that data at one temp. can be superimposed upon data taken at a different temperature
- The amount each reduced modulus has to be shifted along the logarithmic time axis in making the master curve, the socalled shift factor, is a function of temp.

$$
\int \frac{\text{Log } a_r = \log \frac{t}{t(T_g)} = \frac{-17.44(T - T_s)}{51.6 + (T - T_s)}}{\text{W.L.} \text{ Ferry Eq.}}
$$

P. 405 Ex 13.3

a

25℃, measuring time 1h 에서 polyisobutylene 의 stress relaxation modulus $\geq 3 \times$ 10^5 N/m² 이다.

J

- (a) time 1h, 80℃에서 modulus 는?
- (b) 식(13.70)에서 그리고 PIB 의 Tg =197k

$$
\log a(273 + 25) = \frac{-17.44(298 - 197)}{51.6 + 101}
$$

$$
= \frac{-1760}{152.6} = -11.5
$$

$$
\log a \frac{273 - 80}{193} = \frac{17.44 \times 4}{51.6 - 4} = \frac{70}{47.6} = 1.5
$$

$$
\log \frac{a(193)}{a(298)} = 1.5 + 11.5 = 13.0 \quad \left(\log \frac{a(298)}{a(193)} = -13\right)
$$

∖

the master curve at t \approx 10-13 에서의 modulus 는 약 2×10^9 N/m²