

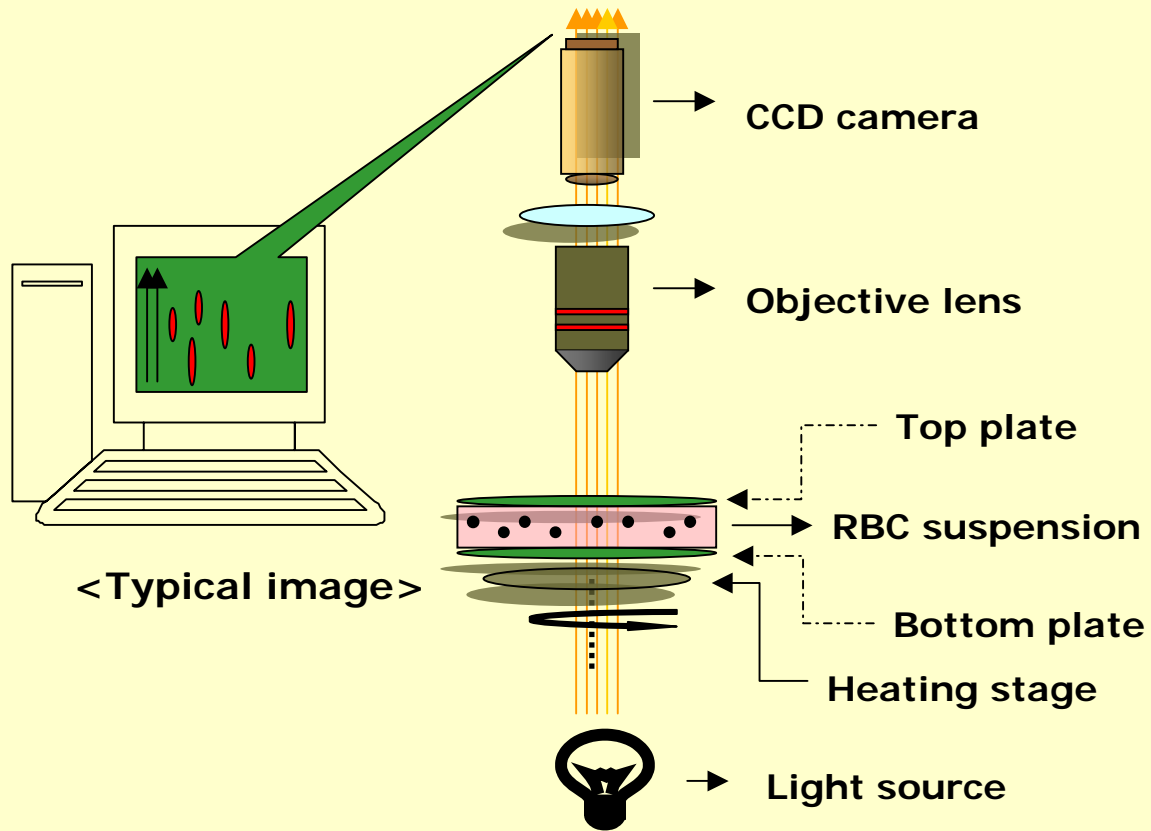
# Ch 03

## Methodology

# Structural probes

- Microscopy (w/ shearing system)
- Small angle light scattering
- Polarimetry (birefringence)
- Dichroism
- Light, X-ray, neutron scattering
- Others

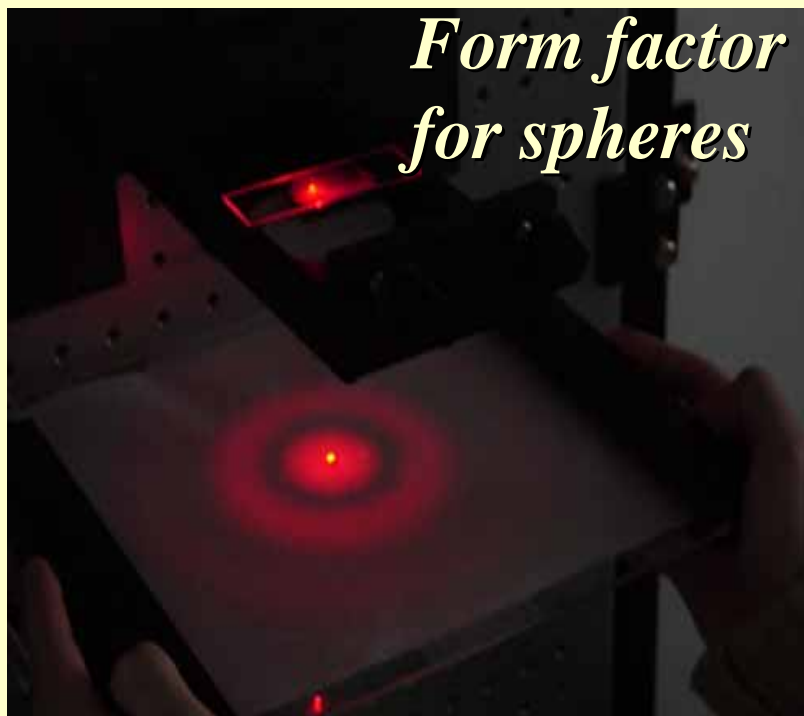
# Shearing system



Shearing system

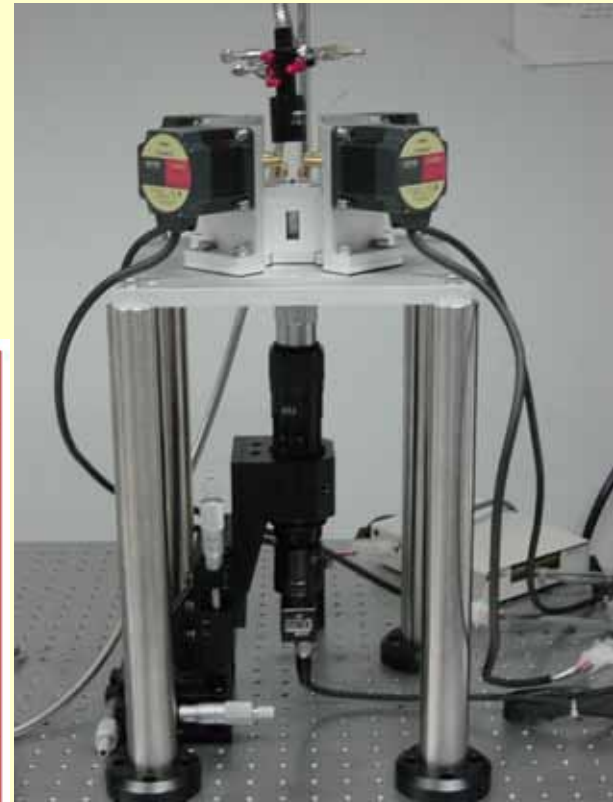
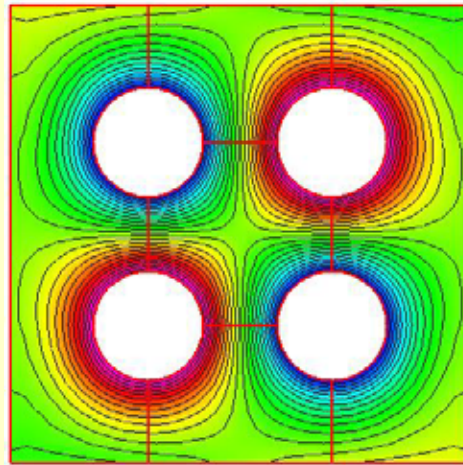
↓  
↑  
→ 10 ~ 100  $\mu\text{m}$

# SALS



# Four roll mill

- Relatively easy to control
- Flow type constant
  - Pure extensional flow:  $\alpha=1$
  - Mixed flow :  $0 < \alpha < 1$
  - Pure shear flow:  $\alpha=0$



# Computational methods

- **Macroscopic simulation**
  - FEM, FVM, spectral...
- **Microscopic simulation**
  - BD, MD, MC, SD, FPD, DPD, LB...
- **Micro-macro simulation**

# Macroscopic simulation

- **Governing eqn's.**

$$\boldsymbol{\tau}_p = f(\mathbf{u}, \boldsymbol{\tau}_p, \lambda, \beta, \eta)$$

$$\text{Re} \left( \frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) = -\nabla p + \nabla \cdot \boldsymbol{\tau}_p + (1 - \beta) \nabla^2 \mathbf{u}$$

$$\beta = \frac{\eta_p}{\eta_p + \eta_s}$$

$$\nabla \cdot \mathbf{u} = 0$$

$$\boldsymbol{\tau}_p + \text{We} \left( \frac{\partial \boldsymbol{\tau}_p}{\partial t} + \mathbf{u} \cdot \nabla \boldsymbol{\tau}_p - (\nabla \mathbf{u})^T \cdot \boldsymbol{\tau}_p - \boldsymbol{\tau}_p \cdot \nabla \mathbf{u} \right) = \beta \left( \nabla \mathbf{u} + (\nabla \mathbf{u})^T \right)$$

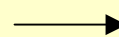
- **Dimensionless Group**

$$\text{Re} = \frac{LU \rho}{\eta} \quad \square \quad \frac{\textit{inertia}}{\textit{viscous}}$$

$$\text{We} = \frac{U \lambda}{L} \quad \square \quad \frac{\textit{elastic}}{\textit{viscous}}$$

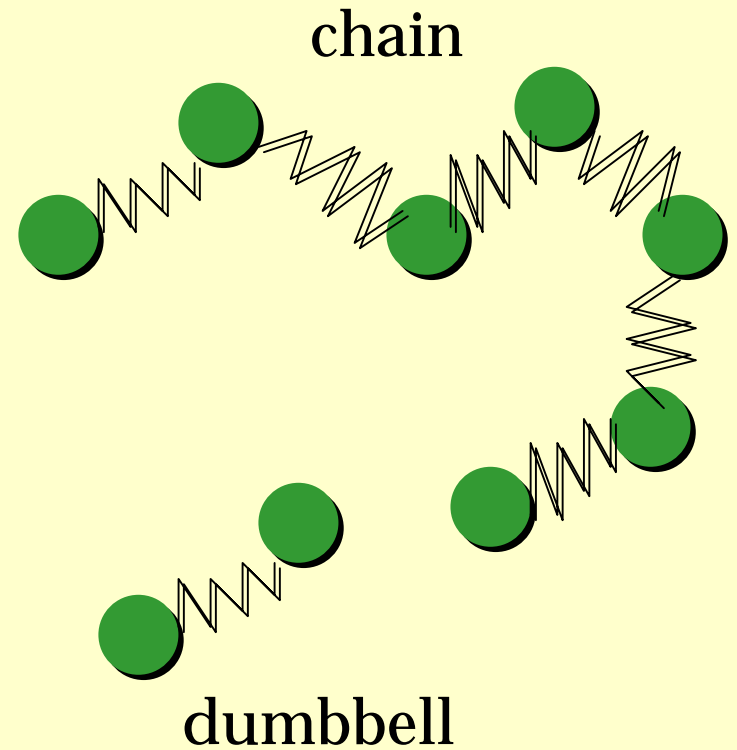
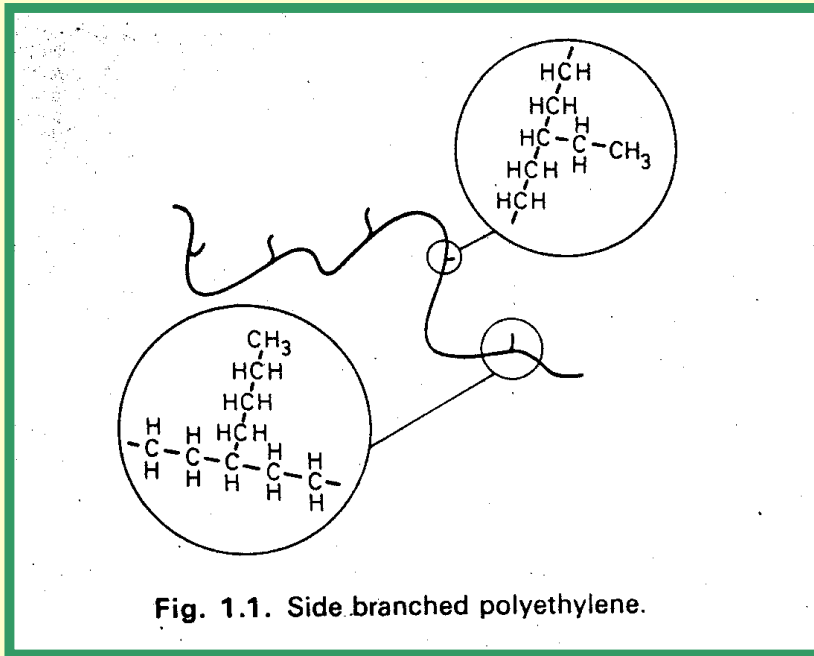
- ◆ **HWNP (High Weissenberg Number Problem)**

- coupled elliptic-hyperbolic system
- ill-posed problem
- geometry effect (singularity)



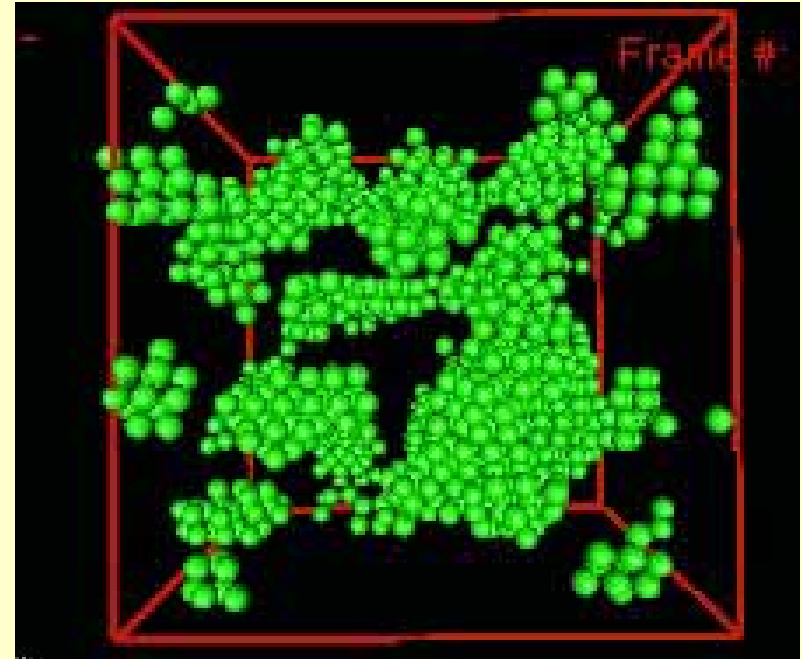
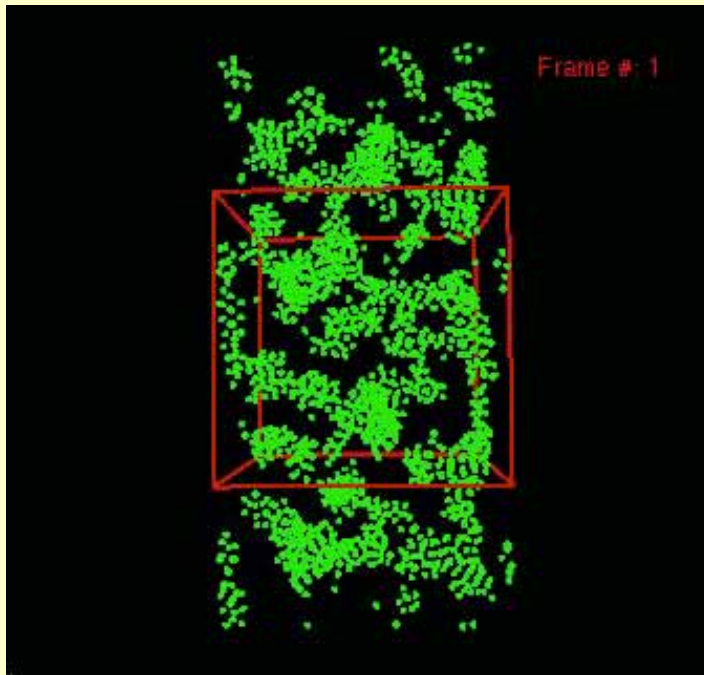
Numerical breakdown

# Microscopic modeling

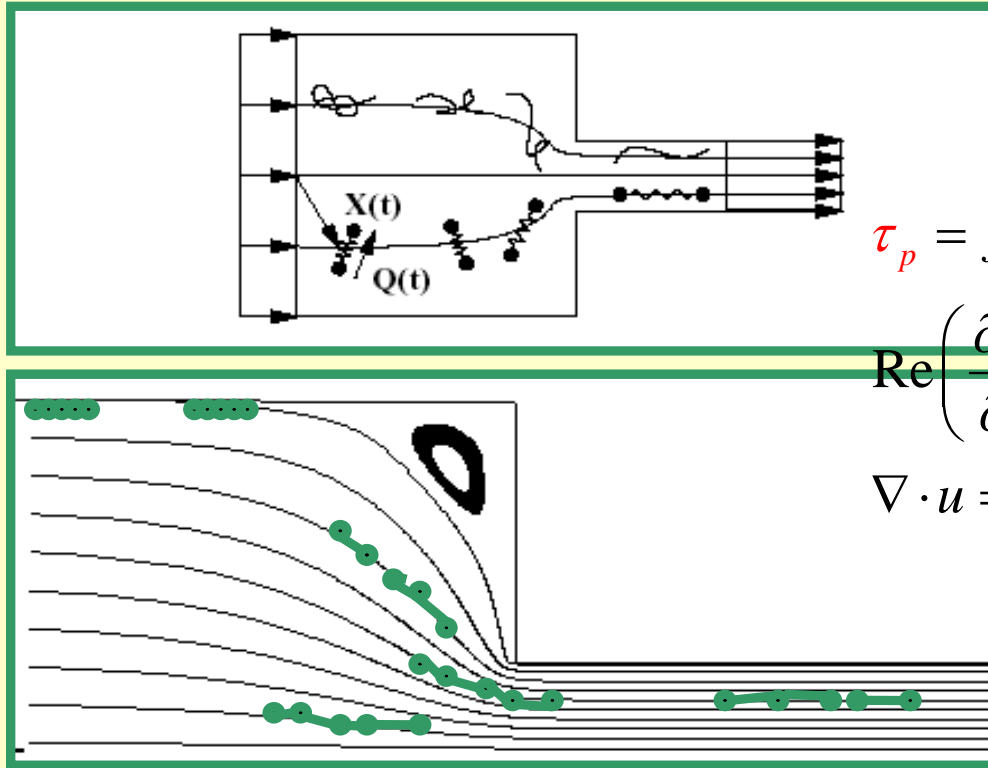




# Modeling: BD, DPD, FPD, LB,...



# Micro-macro simulation



$$\tau_p = f(\mathbf{u}, \tau_p, \lambda, \beta, \eta)$$

$$\text{Re} \left( \frac{\partial u}{\partial t} + u \cdot \nabla u \right) = -\nabla p + \nabla \cdot \tau_p + (1 - \beta) \nabla^2 u$$

$$\nabla \cdot u = 0$$

**Critical to precise process control**

- precision injection, coating, micro-channel flow ...