Lecture 15. Crystallization - Crystal Geometry and Thermodynamics

- Type of Crystallization
- Industrial Example: Production of $MgSO_4$ \cdot 7 H_2 O
- Crystal Geometry
	- Crystal habit
	- Crystal-size distributions
	- Mean particle sizes
- Thermodynamics
	- Solubility and mass balances
	- Energy balances

Crystallization

- A solid-fluid separation operation in which crystalline particles are formed from a homogeneous fluid phase
- One of the oldest separation operations: recovery of NaCl as salt crystals from seawater
- Factors for crystallization
	- Cooling the solution
	- Evaporating the solvent
	- Addition of a second solvent

- when water is the additional solvent: watering-out
- when an organic solvent is added to an aqueous salt solution: salting-out
- fast crystallization called precipitation can occur

Type of Crystallization

• Solubility curves

crystallization

(b) Eutectic-forming system of ortho- and parachloro-

nitrobenzene system suitable for melt crystallization (c) Solid-solution system suitable for fractional melt crystallization

Industrial Example

• Production of $MgSO_4$ -7 H_2O

Evaporation in one or more vessels (effects) to concentrate solution

Partial separation and washing of the crystals from the resulting slurry (magma) by centrifugation or filtration

Drying the crystals to a specified moisture content

Crystal Geometry

• Crystalline and amorphous states

Crystal Habit (1)

- When crystals grow, they form polyhedrons with flat sides and sharp corners (if unhindered by other surfaces such as container walls and other crystals)
- Crystals are never spherical in shape
- Law of constant interfacial angles (Hauy, 1784)
	- The angles between corresponding faces of all crystals are constant, even though the crystals vary in size and in the development of the various faces
	- Crystal habit
	- The interfacial angles and lattice dimensions can be measured by X-ray crystallography

Crystal Habit (2)

• Crystals of a given substance and a given $\frac{c_{\text{rystal form of the seven crystal systems}}{n}$ system exhibit markedly different appearances when the faces grow at different rates, particularly when these rates vary greatly, from stunted growth in one direction to give plates, to exaggerated direction to give plates, to exaggerated
growth in another direction to give needles

Some crystal habits of orthorhombic potassium-sulfate crystals

• Modifications of crystal habit are most often $\begin{bmatrix} \frac{2}{3} \\ \frac{1}{2} \end{bmatrix}$ accomplished by addition of impurities

Crystal Systems and Space Lattices

Simple cubic

Body-centered Face-centered cubic

orthorhombic

tetragonal

Base-centered

orthorhombic

Body-centered

tetragonal

Body-centered orthorhombic

Face-centered orthorhombic

Hexagonal

Base-centered

monoclinic

Triclinic

Sphericity

- Typical magmas from a crystallizer contain a distribution of crystal sizes and shapes
- Characteristic crystal dimension for irregular-shaped particle \rightarrow sphericity, ψ

surface area of a sphere with the same volume as the particle $\psi =$ $\frac{1}{\sqrt{1 - x^2 + y^2}}$ surface area of the particle and shapes

c crystal dimension for irregular-shaped

hericity, ψ

area of a sphere with the same volume as the particle

surface area of the particle
 $\frac{\partial}{\partial \theta}$, $\psi = 1$; for all other particles, $\psi < 1$
 $\frac{\pi D_p^2$ $=\frac{\text{surface area of a sphere with the san}}{\text{surface area of the}}$
a sphere, $\psi = 1$; for all other particl
 $\frac{p}{p}$
 $=\frac{\pi D_p^2}{(\pi D_p^3/6)} = \frac{6}{D_p}$ cal magmas from a crystallizer contain a distributed sizes and shapes
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 D surface area of the particle
 D $\psi = 1$; for all other particles, $\psi < 1$
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 $\frac{6}{D_p} \left(\frac{v_p}{s_p} \right)_{\text{particle}}$ icle \rightarrow sphericity, ψ
 $\psi = \frac{\text{surface area of a sphere with the same volume as the surface area of the particle}}{\text{surface area of the particle}}$

or a sphere, $\psi = 1$; for all other particles, $\psi < 1$
 $\frac{S_p}{\psi_p}$
 $\Rightarrow \psi = \frac{\pi D_p^2}{(\pi D_p^3/6)} = \frac{6}{D_p}$
 $\Rightarrow \psi = \frac{6}{D_p} \left(\frac{v_p}{s_p}\right)_{\text{particle}}$

For a sphere, $\psi = 1$; for all other particles, $\psi < 1$

Stal sizes and shapes

\naracteristic crystal dimension for irregular–
\nricle → sphericity, ψ

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\psi = \frac{\text{surface area of a sphere with the same volume}}{\text{surface area of the particle}}
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\Rightarrow ψ = \frac{6}{D_p} \left(\frac{v_p}{s_p}\right)_{\text{particle}}
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\Rightarrow \psi = \frac{6}{D_p} \left(\frac{v_p}{s_p} \right)_{\text{particle}}
$$

Crystal Size Distributions (1)

• Crystal-size distributions are most often determined with wire-mesh screens: crystal size is taken to be the screen aperture (opening) through which the crystal just passes

Mechanical shaking of a stack of ordered screens is used in sieving operations

• Screen analysis: particlesize-distribution data

* Crystal of Na₂SO₄·10H₂O grown at 18°C during a residence time of 37.2 minutes in a well-mixed laboratory cooling crystallizer

Crystal Size Distributions (2)

• Differential screen analysis: made by $10^{-0.5}$ determining the arithmetic-average $\qquad \qquad$ _{0.4} aperture for each mass fraction that
passes through one screen but not
the next
 $\sum_{\frac{3}{2} 0.2}^{\frac{5}{2} 0.2}$ passes through one screen but not the next

Nominal particle size for that mass fraction

Crystal Size Distributions (3)

• Cumulative screen analysis: plot of cumulative-weight-percent oversize or undersize as a function of screen aperture

- $-$ The curves are mirror images of each other, crossing at a median size where 50 wt% is larger in size and 50 wt% is smaller
- $-$ If a wide range of screen aperture is covered, a log scale for aperture is preferred

Mean Particle Sizes (1)

• Specific surface area (area/mass) of a particle

Mean Particle Sizes (1)
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$$
A_w = s_p / m_p = s_p / v_p \rho_p
$$
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$$
A_w = 6 / \psi \rho_p D_p
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$$
A_w = \sum_{i=1}^n \frac{6x_i}{\psi \rho_p D_p} = \frac{6}{\psi \rho_p} \sum_{i=1}^n \frac{x_i}{D_p} = \frac{x_i \cdot \text{mass fraction}}{b_n \cdot \text{average aperture}}
$$
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$$
A_w = \frac{6}{\psi \rho_p \overline{D_s}}
$$
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$$
face-mean diameter = \overline{D_s} = \frac{1}{\sum_{i=1}^n \frac{x_i}{D_p}} = \frac{x_i \cdot \overline{D_s}}{\sum_{i=1}^n \frac{x_i}{D_p}}
$$
\n
$$
i g h t \text{ or mass-mean diameter} = \overline{D_w} = \sum_{i=1}^n x_i \overline{D_p}
$$

• Surface-mean diameter
$$
\overline{D}_s = \frac{1}{\sum_{i=1}^n \frac{x_i}{\overline{D}_{p_i}}}
$$

• Weight or mass-mean diameter

$$
\frac{\mathbf{1}}{\overline{D}_{p_i}}
$$
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$$
\overline{D}_{W} = \sum_{i=1}^{n} x_i \overline{D}_{p_i}
$$

Mean Particle Sizes (2)

• Arithmetic-mean diameter

 $1\left(\mathbf{v}_{p_i}\right)$ *i J*

 $=1$ $\left\langle \begin{array}{c} \mathbf{D}_{p_i} \end{array} \right\rangle$

 $i=1$ $\left\langle \begin{array}{c} \mathbf{D}_{p_i} \end{array} \right\rangle$

Mean Particle Sizes (3) **Mean Particle Sizes**

mean diameter
 $\sum_{i=1}^{3} N_i = \sum_{i=1}^{n} (f_v \bar{D}_{p_i}^3) N_i$ **Mean Particle Si**:
 1 $N_i = \sum_{i=1}^n (f_v \overline{D}_{p_i}^3) N_i$
 1 value of f_v **Mean Particle Si**
an diameter
 $\sum_{i=1}^n N_i = \sum_{i=1}^n \left(f_v \overline{D}_{p_i}^3 \right) N_i$ **Mean Particle Sizes (3)**
 e -mean diameter
 $\sum_{i=1}^{n} N_i = \sum_{i=1}^{n} (f_v \overline{D}_{p_i}^3) N_i$

constant value of f **Mean Particle S**
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 $\sum_{i=1}^{n} N_i = \sum_{i=1}^{n} (f_v \overline{D}_{p_i}^3) N_i$
 And value of f_v Mean Particle Sizes (3)
 ne-mean diameter
 $f_v \overline{D}_\nu^3 \Big) \sum_{i=1}^n N_i = \sum_{i=1}^n \left(f_v \overline{D}_{p_i}^3 \right) N_i$

constant value of f_v
 $\sum_{i=1}^n \left(\sum_{i=1}^n N_i \overline{D}_{p_i}^3 \right)^{1/3}$ **1ean Particle Sizes (3)**

 N_i = $\sum_{i=1}^{n} (f_i \bar{D}_{p_i}^3) N_i$

value of f_v
 $N_i \bar{D}_{p_i}^3$
 $\left(\sum_{i=1}^{n} N_i\right)^{1/3}$ **Mean Particle Sizes (3)**

mean diameter
 $\sum_{i=1}^{n} N_i = \sum_{i=1}^{n} (f_i \overline{D}_{p_i}^3) N_i$

ttant value of f_v
 $\left(\sum_{i=1}^{n} N_i \overline{D}_{p_i}^3\right)^{1/3}$

• Volume-mean diameter

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\left(f_{\nu}\overline{D}_{\nu}^{3}\right)\sum_{i=1}^{n}N_{i}=\sum_{i=1}^{n}\left(f_{\nu}\overline{D}_{p_{i}}^{3}\right)N_{i}
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$$
\overline{D}_{V}=\left(\frac{\sum_{i=1}^{n}N_{i}\overline{D}_{p_{i}}^{3}}{\sum_{i=1}^{n}N_{i}}\right)^{1/3}
$$

For a constant value of f_v

ume-mean diameter
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(f_v \overline{D}_v^3) \sum_{i=1}^n N_i = \sum_{i=1}^n (f_v \overline{D}_{p_i}^3) N_i
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\na constant value of f_v
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\overline{D}_v = \left(\frac{\sum_{i=1}^n N_i \overline{D}_{p_i}^3}{\sum_{i=1}^n N_i} \right)^{1/3}
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\overline{D}_v = \left(\frac{1}{\sum_{i=1}^n \overline{D}_{p_i}^3} \right)^{1/3}
$$

Solubility and Mass Balances (1)

- Important thermodynamic properties for crystallization: melting point, heat of fusion, solubility, heat of crystallization, heat of solution, heat of transition, specific heat, and supersaturation
- Solubility of just slightly or sparingly soluble or almost insoluble compounds is expressed as an equilibrium constant, called the solubility product for dissolution, by the law of mass action in terms of ion concentration **30 OUDILITY and Mass Balances (1)**

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in concentration
 $\mathbf{Q}_{3(s)} \Leftrightarrow \mathbf{Al}_{(aq)}^{3+} + 3\mathbf{OH}_{(aq)}$
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solution, by the law of mass
on
 $\beta\textbf{OH}^{\cdot}_{\text{(aq)}}$
 $\alpha\textbf{H}^{\cdot+}_{\text{(aq)}}$)³
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ds is expressed as an equilibrium constant,
 *a*_{3(s)} \Leftrightarrow **A**1_(aq) A _{3(aq)} + **3OH**_(aq)
 $a_{Ai^*})(c_{OH^-})^3 = (c_{Ai^{3*}})(c_{OH^-})^3$

paringly soluble compounds, the equilibrium

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bility product for dissolution, by the law of mass action in
s of ion concentration
 $A[(OH)_{3(s)} \Leftrightarrow Al_{(aq)}^{3+} + 3OH_{(aq)}^{*}$
 $K_c = \frac{(c_{Al^*})(c_{OH^-})^3}{a_{Al(OH)_3}} = (c_{Al^*})(c_{OH^-})$ unds is expressed as an equilibrium constant, called
y product for dissolution, by the law of mass action
f ion concentration
 $\text{OH}_{3(s)} \Leftrightarrow \text{Al}_{(aq)}^{3+} + 3\text{OH}_{(aq)}$
 $= \frac{(c_{\text{Al}^{3+}})(c_{\text{OH}^{-}})^3}{a_{\text{Al(OH)}_3}} = (c_{\text{Al}^{3+}})(c$

as of ion concentration
\nAl(OH)_{3(s)}
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\Leftrightarrow
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 Al³⁺_(aq) + 3OH_(aq)
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$$
K_c = \frac{(c_{Al^{3+}})(c_{OH^-})^3}{a_{Al(OH)_3}} = (c_{Al^{3+}})(c_{OH^-})^3
$$

• For less sparingly soluble compounds, the equilibrium constant, K_a , is the more rigorous form compounds, the equilibrium cons

³⁺ $(c_{\text{Al}^{3+}})(\gamma_{\text{OH}^{-}})^3(c_{\text{OH}^{-}})^3$ $\frac{A^{3+}}{a}$ (c_{OH}^3) $=$ $(c_{Al^{3+}}^3)(c_{OH}^3)$
aringly soluble compounds, the equilibrium constant,
nore rigorous form
 $\frac{A^{3+}}{a}$ $\frac{A^{3+}}{a}$ $=$ $(\gamma_{Al^{3+}}^3)(c_{Al^{3+}}^3)(\gamma_{OH}^3)^3$ $(c_{OH}^3)^3$ $\begin{split} &\sum_{\mathbf{A}\mathbf{A}^{3+}})(c_{_{\mathbf{O}\mathbf{H}^{*}}})^{3} \ &\geq \text{compounds, the equilibrium constant} \ &\sum_{\mathbf{A}\mathbf{A}^{3+}})(c_{_{\mathbf{A}\mathbf{A}^{3+}}})(\gamma_{_{\mathbf{O}\mathbf{H}^{*}}})^{3}(c_{_{\mathbf{O}\mathbf{H}^{*}}})^{3} \end{split}$

$$
\mathbf{A}_{c} = \frac{a_{Al(OH)_{3}}}{a_{Al(OH)_{3}}} = (c_{Al^{3+}})(c_{OH^{-}})
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less sparingly soluble compounds, the equ
s the more rigorous form

$$
\mathbf{K}_{a} = \frac{(a_{Al^{3+}})(a_{OH^{-}})^{3}}{a_{Al(OH)_{3}}} = (\gamma_{Al^{3+}})(c_{Al^{3+}})(\gamma_{OH^{-}})^{3}(c_{OH^{-}})^{3}
$$

Solubility and Mass Balances (2)

- Solubility of most inorganic compounds increases with temperature, but a few common compounds (hard salts) exhibit a negative or inverted solubility in certain ranges of temperature, where solubility decreases with increasing temperature
- A change in the solubility curve can occur when a phase transition from one stable hydrate to another takes place

Example of sodium sulfate

- $-$ From 0°C to 32.4°C, $Na₂SO₄$.10H₂O is the stable form and the solubility
increases from 4.8 to 49.5 g
(hydrate–free basis)/100 g H₂O
From 32.4°C to 100°C, Na₂SO₄ is
the stable form and the solubility increases from 4.8 to 49.5 g (hydrate-free basis)/100 g H_2O
- From 32.4 °C to 100 °C, Na₂SO₄ is the stable form and the solubility decreases from 49.5 to 42.5 g/100 \degree . $g H₂O$

Solubility and Mass Balances (3)

- The solubility curve is the most important property for determining the best method for causing crystallization and the ease or difficulty of growing crystals
	- Crystallization by cooling is attractive only
for compounds having a solubility that
decreases rapidly with decreasing
temperature
- For most inorganic compounds, for compounds having a solubility that decreases rapidly with decreasing temperature
	- For most inorganic compounds, crystallization by evaporation is the preferred technique

• Solid compounds with low solubility can be produced by reacting two soluble compounds

- The reaction is so fast that only very fine crystals, called a precipitate, are produced

Energy Balances (1)

- When an anhydrous solid compound, whose solubility increases with increasing temperature, dissolves isothermally in a solvent, heat is absorbed by the solution
- Heat of solution at infinite dilution, ΔH_{sol}° : the amount of heat per mole of compound in an infinite amount of solvent
- For compounds that form hydrates, heat of solution at infinite dilution may be exothermic $(-)$ for the anhydrous form, but becomes less negative and often positive as higher hydrates are When an anhydrous solid compound, whose solubility increases
with increasing temperature, dissolves isothermally in a solvent,
heat is absorbed by the solution
Heat of solution at infinite dilution, $\Delta H_{\text{sol}}^{\alpha}$: the For compounds that form hydrates, heat of solution at infinite
dilution may be exothermic (-) for the anhydrous form, but
becomes less negative and often positive as higher hydrates are
formed by $\mathbf{A} \cdot \mathbf{n} \mathbf{H}_2 \mathbf{$
- As crystals continue to dissolve in a solvent, the heat of solution (integral heat of solution) varies as a function of $\frac{2}{3}$ -10,000 concentration $\text{concentration} \ \cdot \left\{ \text{integral heat of solution at saturation} \right\}$
-

Energy Balances (2)

 \cdot {integral heat of solution at saturation} - {heat of solution at infinite dilution $}$ = {heat of dilution} **Energy Balances (2)**

Equal heat of solution at saturation} – {heat of solution

ite dilution} = {heat of dilution}
 $\Delta H_{\rm sol}^{\rm sat} - \Delta H_{\rm sol}^{\infty} = \Delta H_{\rm dil}$
 $\Delta H_{\rm crys} \approx -\Delta H_{\rm sol}^{\infty}$

Denotes of dilution are
 $\Delta H_{\rm crys$ **Energy Balances (2)**

The set of solution at saturation} - {heat of solution}
 $-\Delta H_{sol}^{\infty} = \Delta H_{dil}$
 $\approx -\Delta H_{sol}^{\infty}$ Heats of dilution are
 $\approx -\Delta H_{sol}^{\infty}$ Heats of dilution are
 $\approx -\Delta H_{sol}^{\infty}$
 $\approx 2\Delta H_{sol}^{\infty}$
 Energy Balances (2)

Equal heat of solution at saturation} - {heat of solution}
 $\Delta H_{\rm sol}^{sat} - \Delta H_{\rm sol}^{\infty} = \Delta H_{\rm dil}$
 $\Delta H_{\rm crys} \approx -\Delta H_{\rm sol}^{\infty}$

by everall energy balance

and the crystallizer
 $\Delta H_{\rm crystal}$
 $\Delta H_{\rm chag}$ **Energy Balances (2)**

eat of solution at saturation} – {heat of

ution} = {heat of dilution}
 $-\Delta H_{sol}^{\infty} = \Delta H_{dil}$
 $\approx -\Delta H_{sol}^{\infty}$

energy balance

energy balance

expostallizer
 ΔH_{sol}^{∞}
 ΔH_{sol}^{∞}
 ΔH_{sol

• An overall energy balance around the crystallizer

$$
m_{\text{feed}} H_{\text{feed}} + Q_{\text{in}}
$$

= $m_{\text{vapor}} H_{\text{vapor}}$
+ $m_{\text{liquid}} H_{\text{liquid}}$
+ $m_{\text{crystals}} H_{\text{crystals}}$

Heats of dilution are

relatively small

