#### Lecture 6. Kinetics and Transport in Sorption (3)

- Ideal Fixed-Bed Adsorption (Frontal Loading Mode)
- Solute Concentration Distributions in Frontal Loading
  - Mass-transfer zone (MTZ)
- Analytical Solution for Concentration
- Scale-Up Using Constant-Pattern Front

# Ideal Fixed-Bed Adsorption (1)

- Assumptions in ideal (local-equilibrium) fixed bed adsorption (frontal loading mode)
  - Negligible external and internal transport-rate resistances
  - Ideal plug flow
  - Adsorption isotherm beginning at the origin



• The bed is divided into two zones or sections

Upstream of the stoichiometric front, c<sub>f</sub> = c<sub>F</sub>, spent adsorbent is saturated with adsorbate at a loading c<sub>b</sub>\* in equilibrium with c<sub>F</sub>
 Downstream of the stoichiometric front, c<sub>f</sub> = 0, the adsorbent is adsorbate-free

## Ideal Fixed-Bed Adsorption (2)

- After a stoichiometric breakthrough time,  $t_{\rm s},$  the stoichiometric wave front reaches the end of the bed



#### Solute Concentration Distributions in Frontal Loading

• Actual solute concentration distributions of frontal are not ideal



- At t<sub>1</sub>, no part of the bed is saturated
- At t<sub>2</sub>, the bed is almost saturated for a distance L<sub>s</sub> and almost clean at L<sub>f</sub>; beyond L<sub>f</sub>, little mass transfer occurs and the adsorbent is unused The region between L<sub>s</sub> and L<sub>f</sub>: mass-transfer zone (MTZ), where adsorption takes place

 $L_f$  can be taken where  $c_f/c_F = 0.05$ , with  $L_s$  at  $c_f/c_F = 0.95$ 

- At  $t_b$  (breakthrough time), the leading point of the MTZ just reaches the end of the bed Breakthrough concentration can be taken for  $c_f/c_F = 0.05$  or minimum detectable (or maximum allowable) solute concentration in effluent fluid

## **Analytical Solution**

• For an initially clean bed free of solute adsorbate (by Anzelius)

$$\frac{c_f}{c_F} \approx \frac{1}{2} \left[ 1 + \operatorname{erf} \left( \sqrt{\tau} - \sqrt{\xi} + \frac{1}{8\sqrt{\tau}} + \frac{1}{8\sqrt{\xi}} \right) \right]$$
$$\xi = \frac{3k_{c,tot}z}{R_p u} \left( \frac{1 - \varepsilon_b}{\varepsilon_b} \right) \qquad \text{Dimensionless distance coordinate}$$
$$\tau = \frac{3\alpha k_{c,tot}}{R_p} \left( t - \frac{z}{u} \right) \qquad \text{Dimensionless displacement-corrected time coordinate}$$

 Profiles of solute concentration in equilibrium with the average sorbent loading (by Klinkenberg)

$$\frac{c_f^*}{c_F} = \frac{\overline{c}_b}{\overline{c}_b^*} \approx \frac{1}{2} \left[ 1 + \operatorname{erf}\left(\sqrt{\tau} - \sqrt{\xi} - \frac{1}{8\sqrt{\tau}} - \frac{1}{8\sqrt{\xi}}\right) \right] \qquad \begin{array}{l} c_f^* = \overline{c}_b \alpha \\ \overline{c}_b^* \text{ is the loading in equilibrium with } c_F \end{array}$$

## Scale–Up Using Constant–Pattern Front (1)

- Persistent transport-rate resistance eventually limits selfsharpening, and an asymptotic or constant-pattern front (CPF) is developed
  - MTZ becomes constant
  - Curves of  $c_f/c_F$  and  $\overline{c}_b/\overline{c}_b^*$  become coincident



 When the CPF assumption is valid, it can be used to determine the length of a full-scale adsorbent bed from breakthrough curves obtained in small-scale laboratory experiments

Total bed length

#### $L_B = LES + LUB$

Length of an ideal, equilibrium-adsorption section unaffected by masstransfer resistance

$$\text{LES} = \frac{Q_F c_F t_b}{q_F \rho_b A}$$

#### Scale-Up Using Constant-Pattern Front (2)

$$LUB = \frac{L_e}{t_s} (t_s - t_b)$$

$$L_e/t_s : \text{ ideal wave-front velocity}$$

 The stoichiometric time, t<sub>s</sub>, divides the MTZ (e.g., CPF zone) into equal areas (t<sub>s</sub> is equidistant between t<sub>b</sub> and t<sub>e</sub>)

$$t_{s} = \int_{0}^{t_{e}} \left( 1 - \frac{c_{f}}{c_{F}} \right) dt$$
$$LUB = \frac{MTZ}{2}$$

