



Chapter 6. Multiphase Systems

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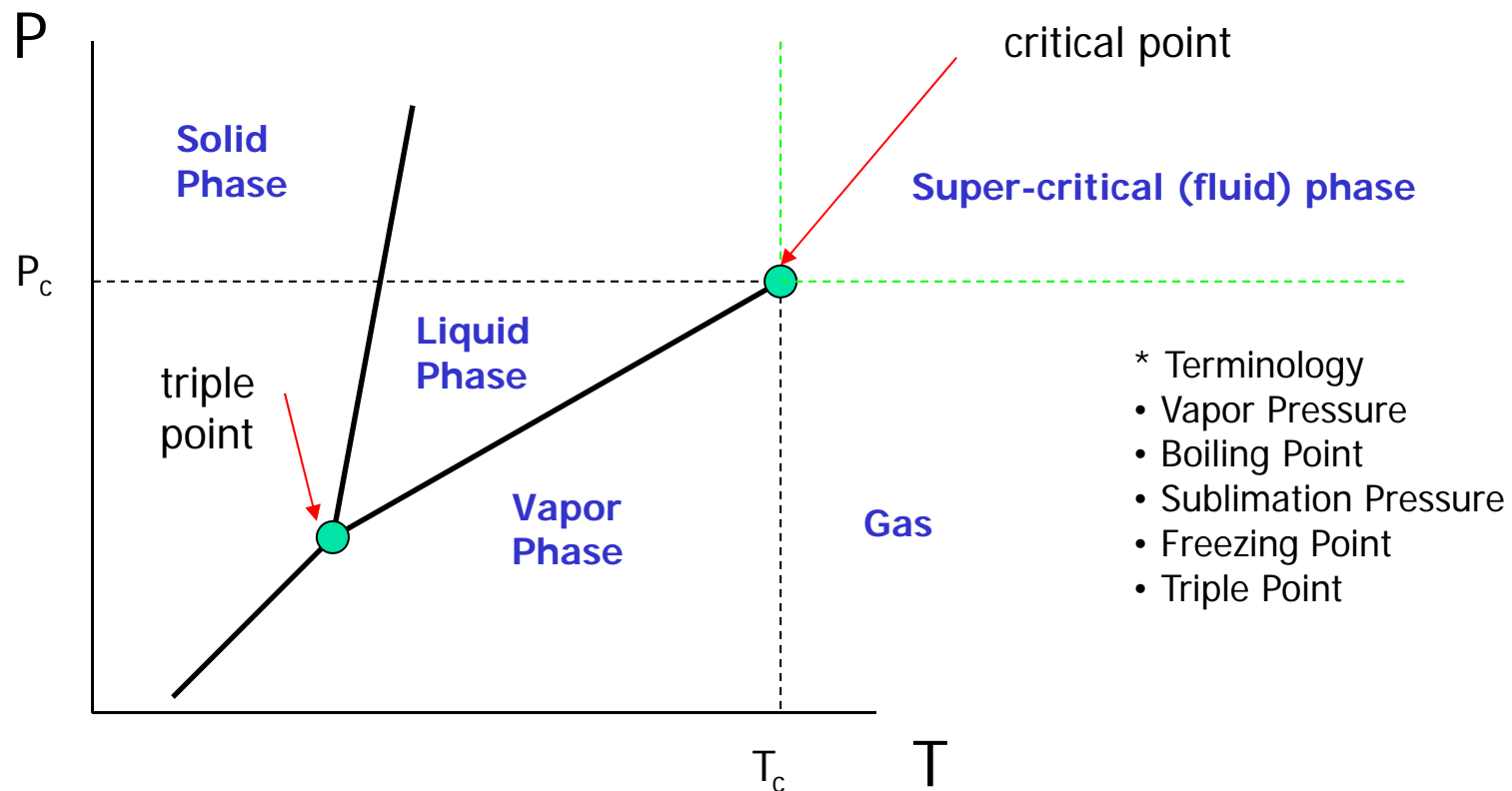


Introduction

- Multiphase systems – Mainly involved in separation process
 - Distillation (증류) : vapor–liquid
 - Driving force of separation : Vapor pressure
 - Crystallization (결정화) : liquid – solid
 - Driving force of separation : solubility
 - Extraction (추출) : liquid – liquid
 - Driving force of separation : distribution coeff.

6.1 Single-Component Phase Equilibrium

■ Phase Diagram





Vapor Pressure

- Source of Vapor Pressure Data
 - Experimental Data from Literature
 - Perry's Handbook
 - Journals (J.Chem.Eng.Data, Fluid Phase Equilibria, ...)
 - Equations and Coefficients : Antoine, ...
 - Perry's Handbook
 - Data Books, Databases , ...
 - From Cox chart (Fig. 6.1-4)
 - Estimation from Clausius – Clapeyron Equation



Clausius–Clapeyron Equation

■ Estimation of Vapor Pressure

$$\frac{dP}{dT} = \frac{\Delta H_v}{T\Delta\hat{V}}$$

→ Enthalpy of Vaporization
→ Volume change of Vaporization (V(gas)-V(liquid))

$$\frac{d \ln P^*}{d(1/T)} = -\frac{\Delta H_v}{R}$$

↓
Integration

$$\ln P^* = -\frac{\Delta H_v}{RT} + B$$

→ This equation can be used as fitting equation for Vapor pressure data.



Vapor Pressure Equations

- Antoine equation (Table 6.1–1)

$$\log_{10} = A - \frac{B}{T + C}$$

- Wagner equation
 - “Properties of Gases and Liquids”

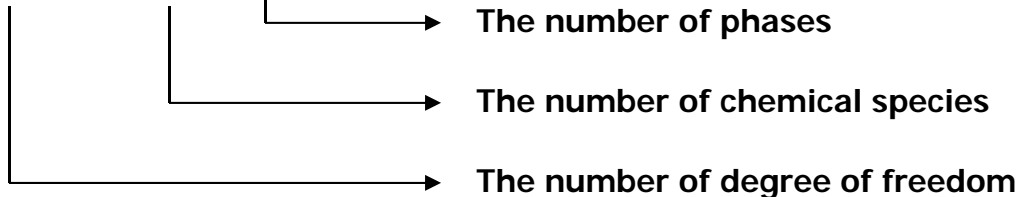
$$\ln P_{vpr} = (A\tau + B\tau^{1.5} + C\tau^3 + D\tau^6) / T_r$$

$$\tau = 1 - T_r$$



6.2 Gibbs Phase Rule

- Types of Process Variables
 - Extensive Variables – depend on the size of the system (N, V,...)
 - Intensive Variables – do not depend on the size of the system (T,P,...)
- Gibbs Phase Rule
 - Degree of freedom for intensive variables

$$F = 2 + m - \Pi$$


The number of phases

The number of chemical species

The number of degree of freedom



Gibbs Phase Rule – Examples

$$F = 2 + m - \Pi$$

- Pure Water

- $F = 2 + 1 - 1 = 2$

(example)
T and P

- Mixture of Ice and Water

- $F = 2 + 1 - 2 = 1$

(example)
T or P

- VLE of acetone + nitrogen

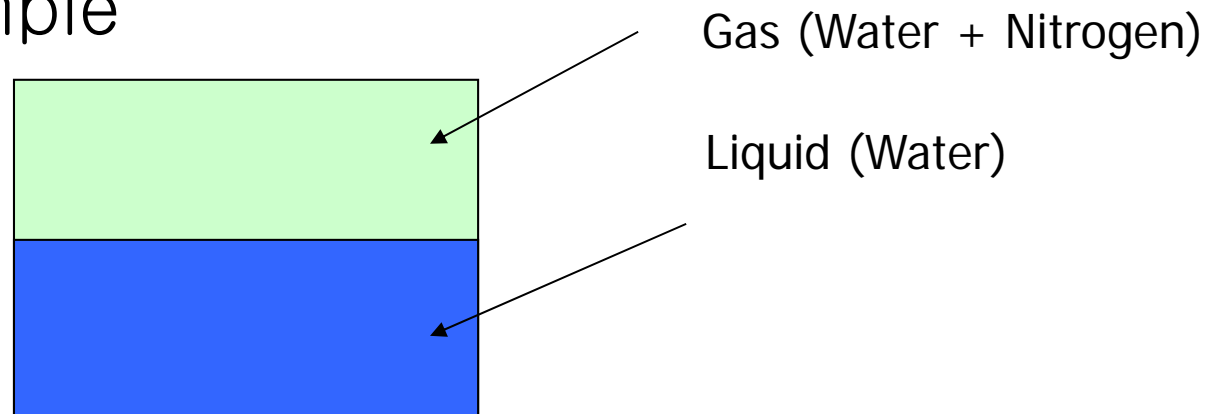
- $F = 2 + 2 - 2 = 2$

(example)
T and x
P and x
T and P
:

Other intensive variables can be calculated
using thermodynamic relations

6.3 Gas-Liquid Systems

- Processes involving gas-liquid systems
 - Evaporation, drying, humidification
 - Condensation, dehumidification
- Example



The gas in GLE is called “**noncondensable**” .
The gas phase is “**saturated**” with water.



GLE-Calculations

- For 2- component GLE
 - Saturation condition, single condensable species

$$p_v = y_v P = p_v^*(T)$$

- Gibbs Phase Rule $F = 2 + m - \Pi$
 - $F = 2 + 2 - 2 = 2$
 - Intensive Variables : y, T, P



Important characteristics of GLE systems

- GLE → gas must be saturated with liquid
- The partial pressure cannot exceed the vapor pressure of the liquid

$$p_v \leq p_v^*(T) \longrightarrow \text{if } p_v > p_v^*(T) \text{ then condensation starts.}$$

- Superheated vapor (과열증기)

$$p_v = y_v P < p_v^*(T)$$

- Dew Point (이슬점)

$$p_v = y_v P = p_v^*(T_{dp})$$

- Degree of Superheat (과열도)

$$= (T - T_{dp})$$



Quantities for GLE systems

- Special case of air+water systems → humidity
- Terminology

- Relative Saturation (Relative Humidity)

$$s_r(h_r) = \frac{p_v}{p_v^*(T)} \times 100\%$$

- Molar Saturation (Molar Humidity)

$$s_m(h_m) = \frac{p_v}{P - p_v} = \frac{\text{moles of vapor}}{\text{moles of vapor} - \text{free(dry) gas}}$$

- Absolute Saturation (Absolute Humidity)

$$s_a(h_a) = \frac{p_v M_v}{(P - p_v) M_{dry}} = \frac{\text{mass of vapor}}{\text{mass of vapor} - \text{free(dry) gas}}$$

- Percentage Saturation (Percentage Humidity)

$$s_p(h_p) = 100 \frac{s_m}{(s_m)^*} = 100 \frac{p_v / (P - p_v)}{p_v^* / (P - p_v^*)}$$



6.4 Multicomponent Gas-Liquid Systems

- Transfer process
 - Gas → Liquid : absorption (흡수)
 - Liquid → Gas : stripping (탈기)
- VLE information
 - From tabulated VLE data
 - Raoult's Law and Henry's Law
 - VLE calculation assuming ideal solution
 - Rigorous VLE calculation using model equations



Raoult's Law and Henry's Law

- Distribution of component between vapor and liquid phase

→ Phase equilibrium thermodynamics

- Simplifications

- Raoult's Law $p_a \equiv y_a P = x_a p_a^*(T)$, $x_a \rightarrow 1$

- Valid for almost pure component. Similar components

- Henry's Law $p_a \equiv y_a P = x_a H_a^*(T)$, $x_a \rightarrow 0$

- Valid for almost dilute component.

- Distribution coefficient $K \equiv y_a / x_a$



VLE calculations for ideal solutions

- Bubble Point temperature calculation
 - Given $P, x \rightarrow$ calculate T, y

$$P = x_a p_a^*(T_{bp}) + x_b p_b^*(T_{bp}) + \dots$$

$$y_i = \frac{x_i p_i^*(T_{bp})}{P}$$

- Dew point temperature calculation
 - Given $P, y \rightarrow$ calculate T, x

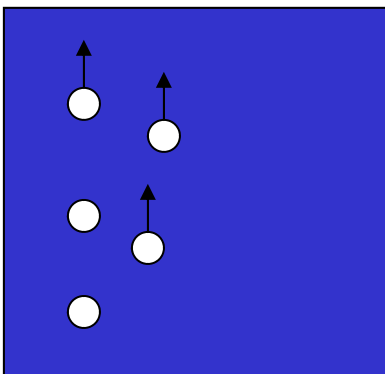
$$x_i = \frac{y_i P}{p_i^*(T_{dp})}$$

$$\sum_i x_i = \sum_i \frac{y_i P}{p_i^*(T_{dp})} = 1$$

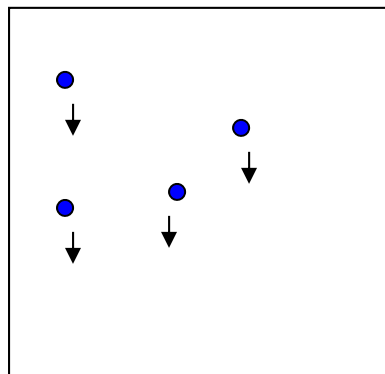


VLE calculations

- Bubble T : $P, x \rightarrow T, y$
- Bubble P : $T, x \rightarrow P, y$
- Dew T : $P, y \rightarrow T, x$
- Dew P : $T, y \rightarrow P, x$



Bubble point



Dew point



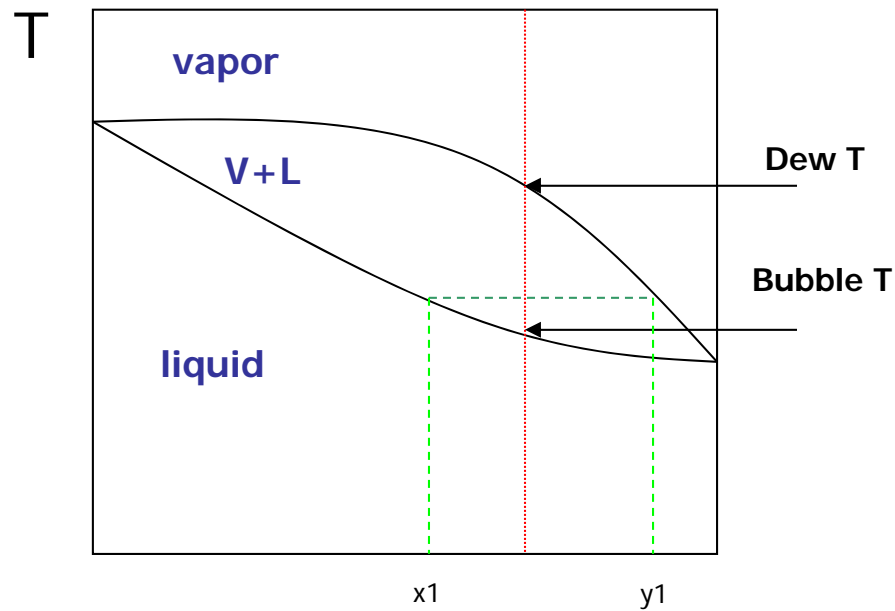
Numerical Methods for the VLE calculations

- Newton – Raphson Method
- Secant Method
- ...

- ← Student presentation

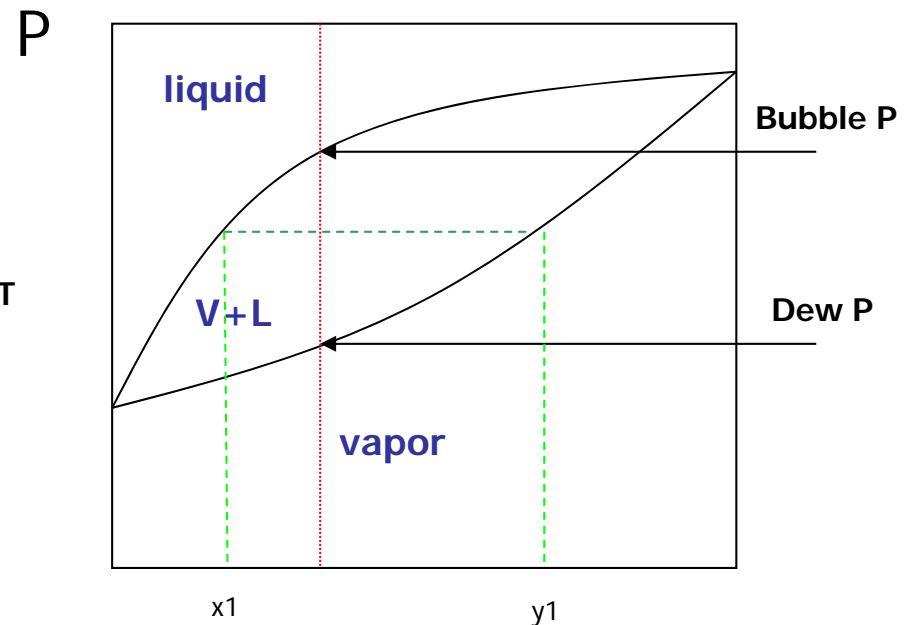
Phase diagrams for binary VLE

■ Txy diagram



x or y

■ Pxy diagram



x or y



Solutions of Solids in Liquids

- Solubility

- Limits on the amount of solids that can be dissolved
- Solubility of a solid depends strongly on T
- Ex)
 - 222 g AgNO₃ / 100 g H₂O at 20 ° C
 - 0.003 g AgCO₃ / 100 g H₂O at 20 ° C
 - 0.00002 g AgBr / 100 g H₂O at 20 ° C

- Crystallization

- Separation of solids and liquids
- Driving force = solubility difference
- A solute in equilibrium with a crystal must be saturated.

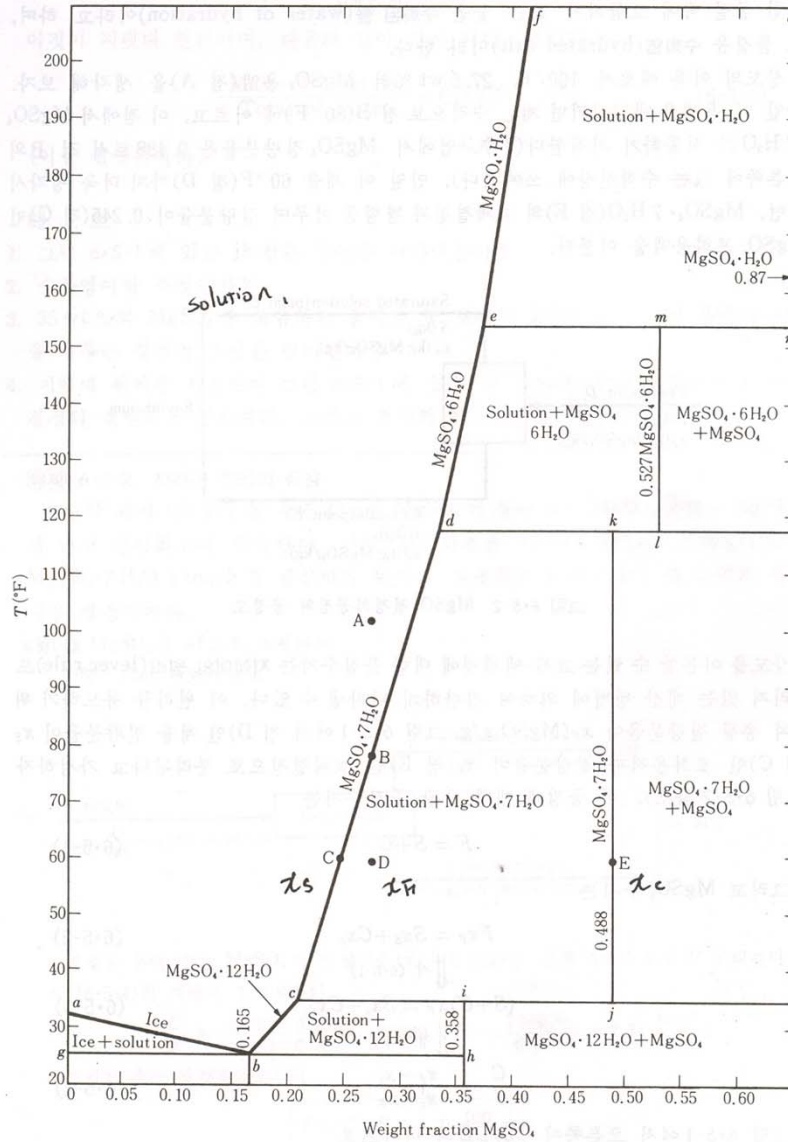


그림 6·5-1 $\text{MgSO}_4\text{-H}_2\text{O}$ 계의 상도

A Phase diagram for solid-liquid system



Phase diagrams for solid–liquid systems

- See figure 6.5–1
- Lever rule (지렛대 원리)

$$F(\text{feed}) = S(\text{solution}) + C(\text{crystal})$$

$$Fx_F = Sx_S + Cx_C$$

$$(S + C)x_F = Sx_S + Cx_C$$

$$\frac{C}{S} = \frac{x_F - x_S}{x_C - x_F} = \frac{\overline{CD}}{\overline{DE}}$$

$$\therefore \frac{C(\text{kg crystal})}{S(\text{kg solution})} = \frac{\overline{CD}}{\overline{DE}}$$



Colligative Solution Properties

- 용액의 총괄성
 - Properties change on a solution
 - Vapor pressure lowering
 - Boiling point elevation
 - Melting point depression
 - Osmotic pressure
 - Depend only on molar concentration
(not on the solute and solvent)



Colligative properties

- Vapor Pressure Lowering

$$p_s(T) = (1-x)p_s^*(T)$$

$$\Delta p_x^* = p_s^* - (p_s^*)_e = xp_s^*$$

- Boiling Point Elevation

$$\Delta T_b = \frac{RT_{b0}^2}{\Delta \hat{H}_v} x$$

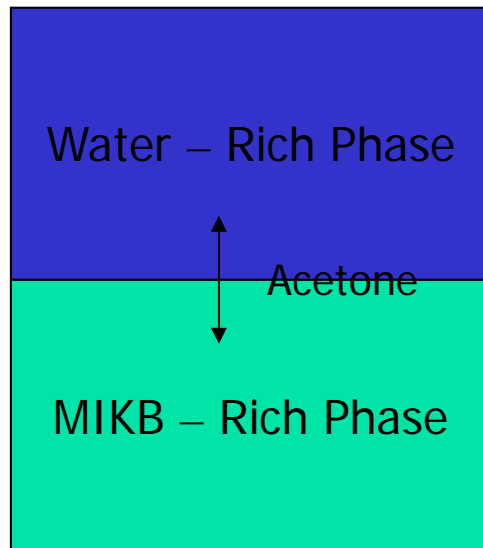
- Melting Point Depression

$$\Delta T_m = \frac{RT_{m0}^2}{\Delta \hat{H}_m} x$$



6.6 Immiscible and Partially Miscible Liquids

- Example) Water + MIBK (Methyl Isobutyl Ketone) + Acetone System



Distribution Coefficient

$$K = \frac{(x)_{MIBK}}{(x)_{WATER}}$$

- Partially miscible liquids
- Immiscible System
- Liquid-Liquid Extraction

Phase diagram for ternary LLE systems

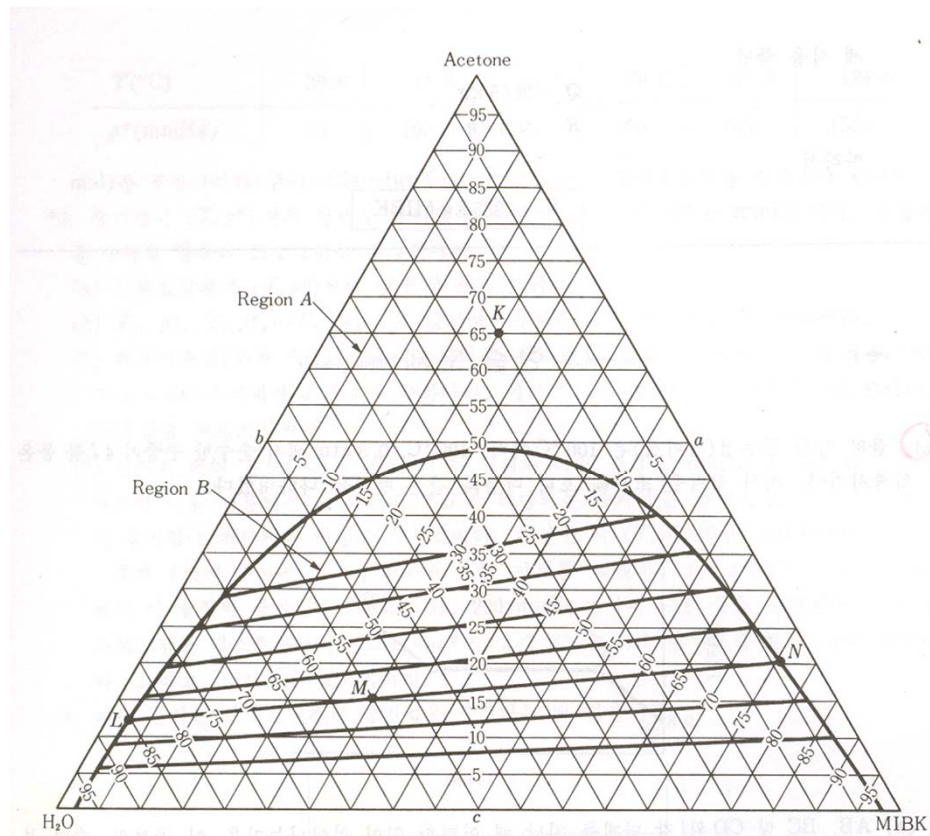


그림 6·6-1 25°C에서 물-아세톤-메틸이소부틸케톤의 삼각상도